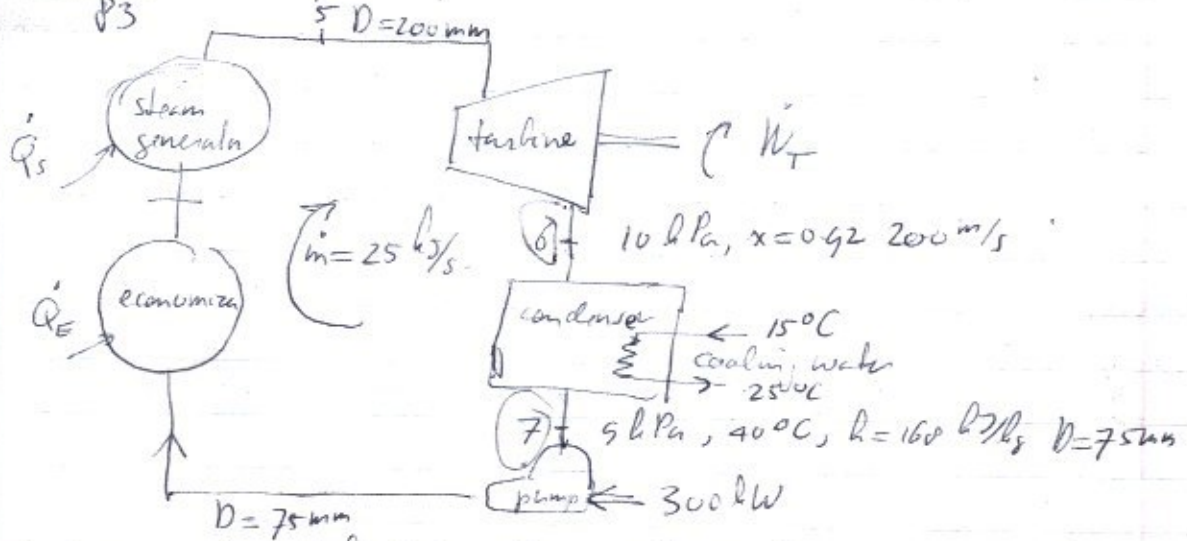


P6.100 Steam power plant



Asked: rate of heat transfer in the condenser, and the mass flow rate of cooling water.

Answer: The heat transfer is from steam in the condenser to cooling water. So we have two control volumes to deal with:
 a) the flow of steam through the condenser; heat Q goes out of this C.V.
 b) the flow of cooling water; heat Q goes into this C.V.

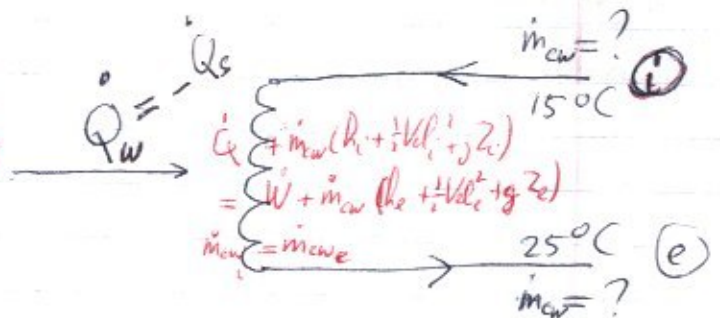
Draw them separately:

$\dot{m} = 25 \text{ kg/s}$ (I)
 10 kPa (II)
 $x = 0.92$ (I)

Tables

condenser except coolant tubing
 $\dot{Q}_c + \dot{m}_s (h_6 + \frac{1}{2} V_6^2 + g z_6)$
 $= \dot{W} + \dot{m}_s (h_7 + \frac{1}{2} V_7^2 + g z_7)$
 $\dot{m}_6 = \dot{m}_7$

9 kPa (I)
 40°C (I)
 $h = 160 \text{ kPa}$ (I)
 $D = 75 \text{ mm}$
 $\dot{m} = \frac{A_7 V_7}{v_7}$



Answer :

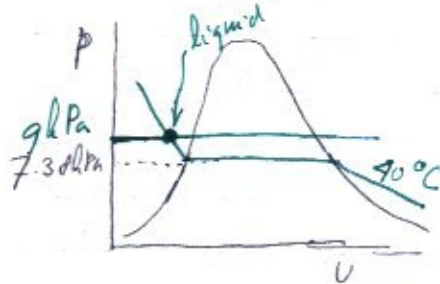
a) I have full info about condenser inflow and outflow, and $\dot{W} = 0$ (no moving parts), so I should be able to figure out \dot{Q} .

State 6: Table B.1.2 @ 10 kPa : $h_f = 191.01 \frac{\text{kJ}}{\text{kg}}$ $h_{g6} = 2390.02 \frac{\text{kJ}}{\text{kg}}$

$$h_6 = h_f + x h_{g6} = 191.01 + 0.52 \cdot 2390.02 \frac{\text{kJ}}{\text{kg}}$$

$$= 2393.20 \frac{\text{kJ}}{\text{kg}}$$

State 7: Do not assume pressure is constant $p_7 = 9 \text{ kPa} \neq p_6$.



9 kPa is not in B.1.4, so use saturated values at 40°C

$$v_7 = 0.001008 \frac{\text{m}^3}{\text{kg}}$$

$$h_7 = 167.59 \text{ (value given at 160)}$$

$$25 \frac{\text{kg}}{\text{s}} = \frac{Vel_7 \frac{\pi}{4} 0.075^2 \text{ m}^2}{0.001008 \frac{\text{m}^3}{\text{kg}}}$$

$$\dot{m}_7 = \frac{Vel_7 A_7}{v_7}$$

Use 1st law: $\Rightarrow Vel_7 = 5.7 \text{ m/s}$

$$\dot{Q}_S + \dot{m}_6 \left(h_6 + \frac{1}{2} Vel_6^2 + g Z_6 \right) = \dot{W} + \dot{m}_7 \left(h_7 + \frac{1}{2} Vel_7^2 + g Z_7 \right)$$

no moving parts

$$\dot{Q}_S + 25 \frac{\text{kg}}{\text{s}} \left(2393.20 \frac{\text{kJ}}{\text{kg}} + \frac{1}{2} 200^2 \frac{\text{m}^2}{\text{s}^2} \frac{1 \text{ kJ}}{1000 \frac{\text{m}^2}{\text{s}^2}} \right)$$

$$= 25 \frac{\text{kg}}{\text{s}} \left(160 \frac{\text{kJ}}{\text{kg}} + \frac{1}{2} 5.7^2 \frac{\text{m}^2}{\text{s}^2} \frac{1 \text{ kJ}}{1000 \frac{\text{m}^2}{\text{s}^2}} \right)$$

$$\Rightarrow \dot{Q}_S = -56130 \text{ kW} \text{ (out of the steam, since negative)}$$

Now know $\dot{Q}_{\text{cool}} = 56130 \text{ kW}$ added to the cooling water

b) Figure out the cooling water.

Note: I do not have pressures for the cooling water!
 Idea: use $h_e - h_i = c_p (T_e - T_i)$. Requires only temperatures.

$$\dot{Q} + \dot{m}_{cw} (h_i + \cancel{\frac{1}{2} V_{el,i}^2} + \cancel{\gamma z_i}) = \dot{m}_{cw} (h_e + \cancel{\frac{1}{2} V_{el,e}^2} + \cancel{\gamma z_e})$$

$\xrightarrow{\text{ignore}}$ $\xrightarrow{\text{ignore}}$ $\xrightarrow{\text{ignore}}$ $\xrightarrow{\text{ignore}}$
 moving parts

$$\dot{Q} \approx \dot{m}_{cw} (h_e - h_i) = \dot{m}_{cw} c_p (T_e - T_i)$$

Table A-3a
 Table A-4: $c_p = 4.18 \frac{\text{kJ}}{\text{kgK}}$ at 25°C, probably

OK at 20° (interpolated: 4.19)

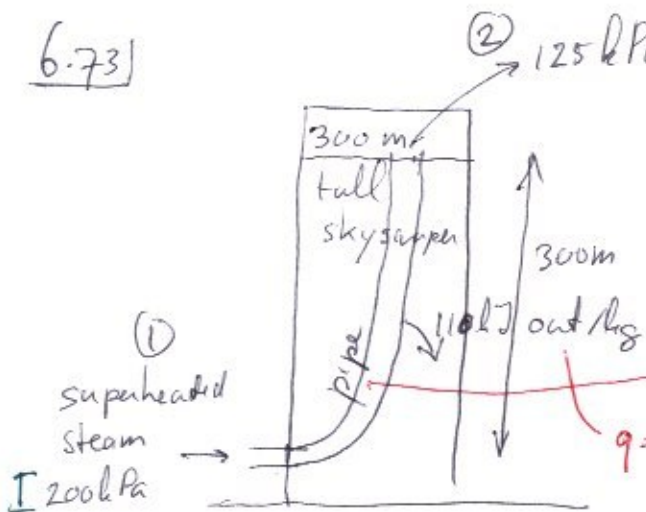
Put in numbers

$$56130 \text{ kW} = \dot{m}_{cw} 4.18 \frac{\text{kJ}}{\text{kgK}} (25 - 15)$$

$$\dot{m}_{cw} = \underline{\underline{1343 \frac{\text{kg}}{\text{s}}}}$$

or $q = c_p (T_2 - T_1)$
 $\dot{Q} = \dot{m} c_p (T_2 - T_1)$
 (same!)

6.73



② 125 kPa I minimum case: just ready to condense at top
 $\rightarrow x=1$
 $m_2 = m_1$
 nothing given about velocities
 $\dot{Q} + \dot{m}_1 (h_1 + \frac{1}{2} V_1^2 + \delta Z_1)$
 $= \dot{Q} + \dot{m}_2 (h_2 + \frac{1}{2} V_2^2 + \delta Z_2)$
 \downarrow
 $q + h_1 + \delta Z_1$
 $= h_2 + \delta Z_2$

Asked: T_1 so that no water condenses in the pipe $h_1 = h_2 - q + \delta(Z_2 - Z_1)$

Solution: $h_1 = h_2 - q + \delta(Z_2 - Z_1)$

Table B.A-5, sat. water P.E. @ 125 kPa: $h_{g2} = h_2 = 2685.35 \frac{kJ}{kg}$
 $(T_2 = 105.97)$

$h_1 = h_2 - q + \delta(Z_2 - Z_1)$
 $= 2685.35 \frac{kJ}{kg} + 110 \frac{kJ}{kg} + 9.81 \frac{m}{s^2} \cdot 300m \cdot \frac{1 \frac{kg}{s^2}}{1000 \frac{m^2}{s^2}}$
 $= 2798.15 \frac{kJ}{kg}$

Table B.A-6, sup. water vap @ 0.2 MPa, $h = 2798 \frac{kJ}{kg}$

$s = 2798$ $s_1 = 2768.8$ $s_2 = 2870.46$
 $d_1 = 150^\circ C$ $d_2 = 200^\circ C$

$T_1 = d_1 + \frac{s - s_1}{s_2 - s_1} (d_2 - d_1) = 150 + \frac{2798 - 2768.8}{2870.46 - 2768.8} (200 - 150)$
 $= 164.5^\circ C$

Throttle flow

6.40

Helium is throttled from 1.2 MPa, 20°C, to a pressure of 100 kPa. The diameter of the exit pipe is so much larger than the inlet pipe that the inlet and exit velocities are equal. Find the exit temperature of the helium and the ratio of the pipe diameters.

Solution:

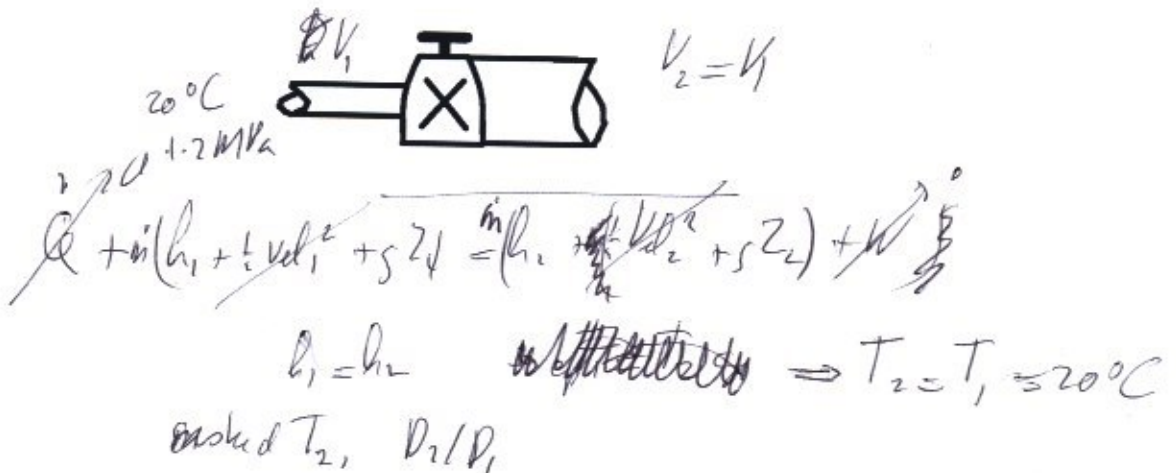
C.V. Throttle. Steady state,

Process with: $q = w = 0$; and $V_i = V_e$, $Z_i = Z_e$

Energy Eq.6.13: $h_i = h_e$, Ideal gas $\Rightarrow T_i = T_e = 20^\circ\text{C}$

$$\dot{m} = \frac{AV}{RT/P} \quad \text{But } \dot{m}, V, T \text{ are constant } \Rightarrow P_i A_i = P_e A_e$$

$$\Rightarrow \frac{D_e}{D_i} = \left(\frac{P_i}{P_e}\right)^{1/2} = \left(\frac{1.2}{0.1}\right)^{1/2} = 3.464$$



$$\frac{A_2 V_2}{R T_2 / P_2} = \frac{A_1 V_1}{R T_1 / P_1}$$

$$\frac{A_2}{A_1} = \frac{P_1}{P_2} = \frac{D_2^2 \sqrt{g}}{D_1^2 \sqrt{g}} \quad \frac{D_2}{D_1} = \sqrt{\frac{P_1}{P_2}} = \sqrt{12} = 3.464$$