Design of a Compact Pressure Sensor for Multi-Layer Insulation in a Vacuum



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Presentation Overview

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Presenter: Jason Carvalho

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Project Scope

The goal of this project is to design and implement a compact pressure sensor that is easily embedded between layers of Multi-Layer Insulation (MLI).
 Rapid Response Time
 The ability to measure a large pressure range

Noninvasive to the MLI

> This interstitial pressure is measured to quantify the heat transfer through the system

> Heat transfer is critical to cryogenic storage and applications in space

Project Objectives

> Develop a pressure sensor with minimal parts

> Minimize the wiring and power consumption of the device

Minimize the heat produced by the sensor

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Project Constraints

Pressure Sensor

- ◆ Be able to measure a pressure as low as 10⁻² Pa
- * Have a minimum response rate of 1 sample per second

Multi-Layer Insulation

- Sensor dimensions shouldn't exceed interlayer spacing
 - ✤ 12 layers is roughly 5 mm

Working environment

- ✤ Temperature conditions range from 293 K to 77 K
- Out gassing
- Vacuum

House of Quality

Table 1 - House of Quality for Pressure Sensor Design



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Capacitor Design

1. Palladium-gold sputtered capacitance tracts





Figure 1: Cross section view of capacitor (left), and exploded view (right)

Presenter: Michael Kiefer

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Multi-Stage Capacitor Design

1: Capacitor top diaphragm:

-High sensitivity – reads low pressures

- -165 µm OD, 125 µm ID diaphragm
- 20 nm thickness, 27 µm deflection at 10 Pa

-Nano-metallic coating to create capacitor plate (sputtering)

2: Silica spacer

3: Intermediate diaphragm:

-Medium to low sensitivity – reads medium to high pressure ranges.

- 50 nm thickness, 28 µm deflection at 150 kPa
- 4: Silica Base plate
- 5: Capacitor bottom plate:

-Rigid metallic plate



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Figure 2: Displays the exploded view of the multi stage capacitor Presenter: Michael Kiefer

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Multi-Stage Capacitor Design

- Cavities formed in the silica base by parabolic germanium doped etching
- Capacitor assembled in a vacuum
- Parts either fused together, or set with a UV-reactive polymer



Figure 3: Multi stage capacitor cross sectional view

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Fiber Optic Design

> 1: Silica diaphragm
 *125 µm OD
 *85 µm ID diaphragm
 > 2: Silica core

3: Lead-in optical fiber
Multimodal or single modal



Figure 5 Cross section view and fully assembled view of Fiber optics sensor

Presenter: Michael Kiefer

Fiber Optics

> Observes change in phase, polarization, transmit time, or wavelength to measure pressure

> Pros

- Good in high vibrational, wet, noisy, corrosive, and extreme heat environments
- Immune to electromagnetic interference
- ✤ Ability to measure a large range of pressures
- High Sensitivity and Bandwidth
- Size (125 micrometers)
- > Cons
 - Relatively difficult design
 - ✤ Cost
 - Assembly requires special equipment



Figure 4 Displays the size of a fiber opticspressure sensorPresenter: Michael Kiefer

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Decision Matrix

 Table 2 - Pugh Decision Matrix for pressure sensor concepts

	Capacitor	Fiber Optics	Multi-Stage Capacitor
Accuracy	0	1	0
Minimal Invasiveness	0	0	0
Heat Production	0	-1	0
Reading Range	0	2	1
Reading Speed	0	0	0
Total	0	2	1

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- Creating the nano-capacitance prototype falls outside of the time restraint and budget
- > To progress with a prototype and testing, scaling must occur
- \blacktriangleright Wish to scale from 125 µm diameter diaphragm to a more pragmatic 25 mm (200x)
 - * Enables the experimentation of capacitance pressure sensors in the previously shown design
 - * Easier implementation with ongoing sensor research directed at temperature detection



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Design Calculations

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Critical minimum thickness of liaphragm at given pressure (P):		of Maximu (P): given P	Maximum deflection at given Pressure (P) and		Critical maximum body pressure at given shell thickness:		$\gamma = 1 - 0.901(1 - e^{-\phi})$ 1 [r]	
$h = \sqrt{\frac{3\pi}{\sigma_y}}$	τr ² * Ρ 4πσ _y d stress	$w_{max} = -\frac{3\pi}{Max}$	$\frac{ss(n)}{r^2 P((1/\mu)^2)}$ $\frac{16\pi Eh(1/\mu)}{16\pi Eh(1/\mu)}$ The pressure during	$\frac{(-1)r^2}{t^2}$	$p = \frac{0.855}{(1 - \mu^2)^2}$ kPa	$\frac{1}{\frac{3}{4}} * \frac{E\sqrt{\gamma}}{\left(\frac{r}{t}\right)^{\frac{5}{2}} * \frac{l}{r}}$	$\varphi = \frac{1}{16}\sqrt{t}$ $\mu = Poisson's Ratio$ $E = Young's Modulus$ $r = diaphragm radius$ $l = sensor length$ $t = shell thickness$	
	Diaphragm Diameter	Min. Thickness (@150 kPa)	Design Thickness	Safety Factor	Critical Diaphragm Pressure	Maximum Deflection (@150kPa)	Shell Thickness	Critical Body Pressure
Prototype	25 mm	0.05 mm	0.10 mm	2.00	600 kPa	5.60 mm	5 mm	20 MPa
Actual Sensor	125 µm	0.25 μm	0.50 µm	2.00	600 kPa	28.0 µm	20 µm	400 MPa

Prototype Production

- Silicone diaphragm acquired (0.1mm and 0.2 mm)
- Epoxy capacitor base finished using HIPS dissolvable filament



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Prototype Production

- Use SEM lab to sputtering tracts onto silicone
- > UV polymer to adhere the diaphragm





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Experimental Testing

- Capacitance is a function of geometry (area and distance apart)
- Each capacitor has a resonant frequency that can be determined using a network analyzer and oscilloscope
- > Network analyzer creates electromagnetic fields, which will cause voltage to oscillate in the capacitor
- Voltage read at the capacitor positive will decrease when resonance has been achieved at the dictated frequency





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Budget

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Total Budget: \$500

- Electronics: \$55
- Silicone: \$40
- ➢ Epoxy: \$60
- ➢ HIPS Filament: \$45

Updated Gantt Chart

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Future Work

Purchase Masterbond UV10 epoxy

Interface sensor with network analyzer

Calibrate sensor

Determine viability

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Questions?