

# Team 24

## Magnetically Coupled Pump/Mixer System for Cryogenic Propellant Tank Destratification Final Presentation

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### Sponsor:

NASA Marshall Space Flight Center  
Florida Space Grant  
AME Center

### Advisor:

Dr. Wei Guo

### Instructors:

Dr. Shih and Dr. Gupta



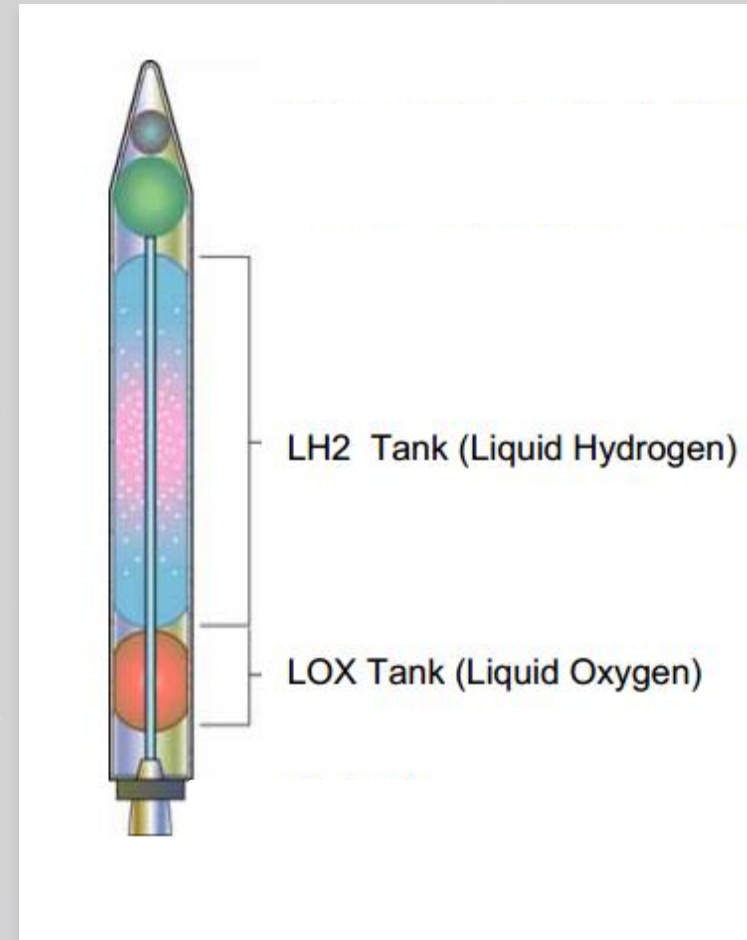
# Agenda

- Background, Motivation, and Project Definition
- Prototype Design and Assembly
- Analyses
- Design of Experiment and Results
  - Water and LN Testing
- Project Management
- Future Improvements
- Conclusion



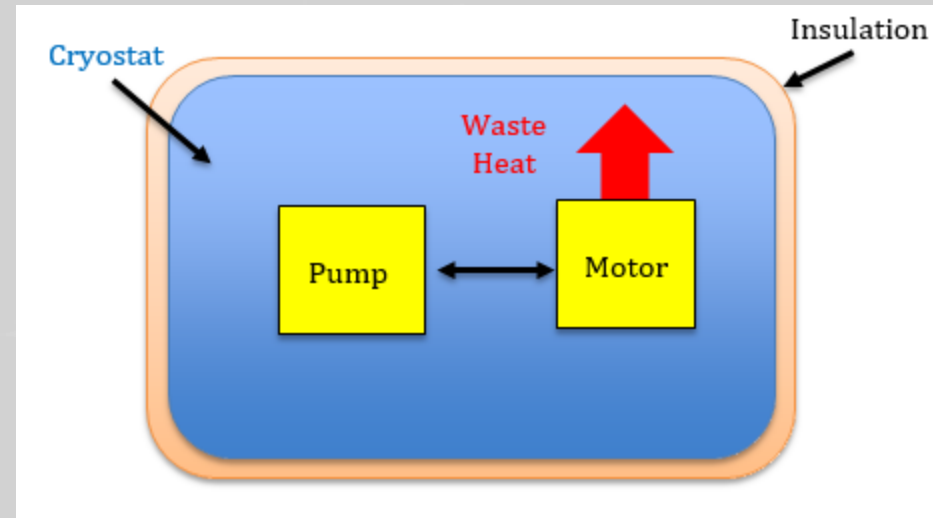
# Background

- Cryogenics used as rocket fuel
  - Excess cryogenics must be stored
- Issues with long term storage of cryogenics
  - Stratification
  - Pressure control
  - Venting
- Mixing the propellants
  - Destratification
  - More time before venting



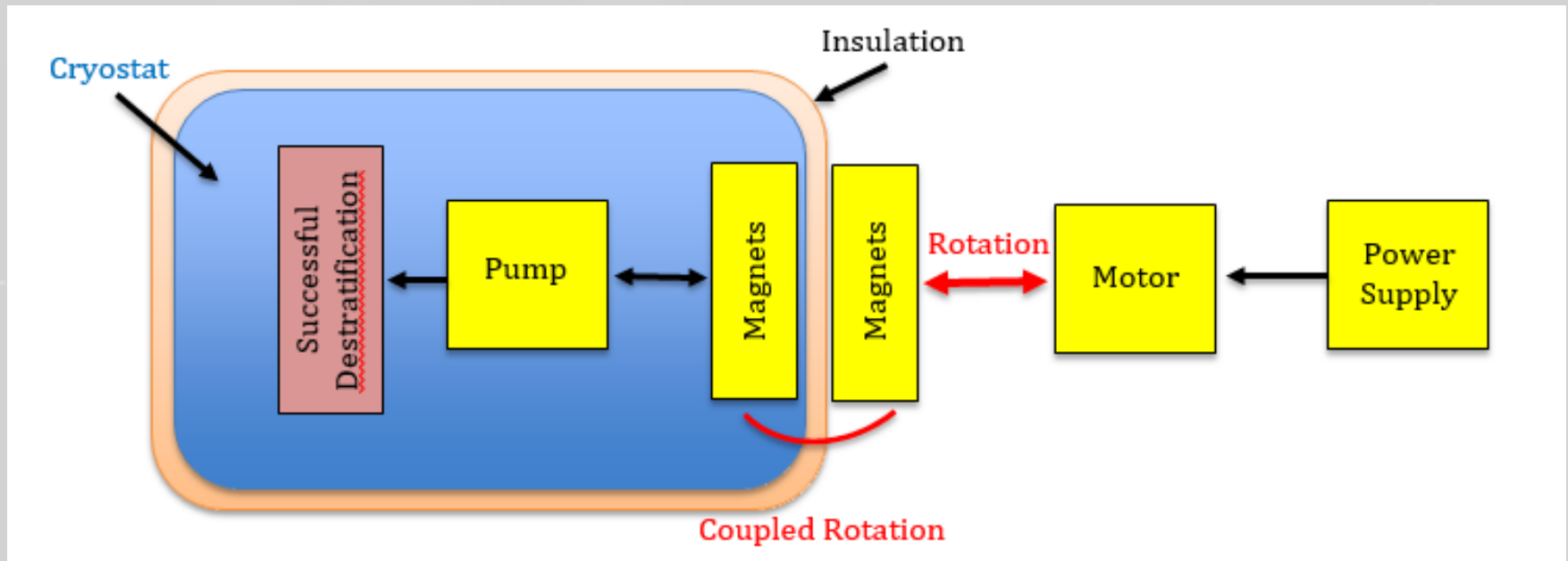
# Motivation

- Current system
  - Various AC single and 3 phase motors
  - Waste heat added to cryogenics
  - Motor couple to a pump operating in submerged conditions
- Designed system
  - Remove waste heat through magnetic coupling



Block diagram of current system

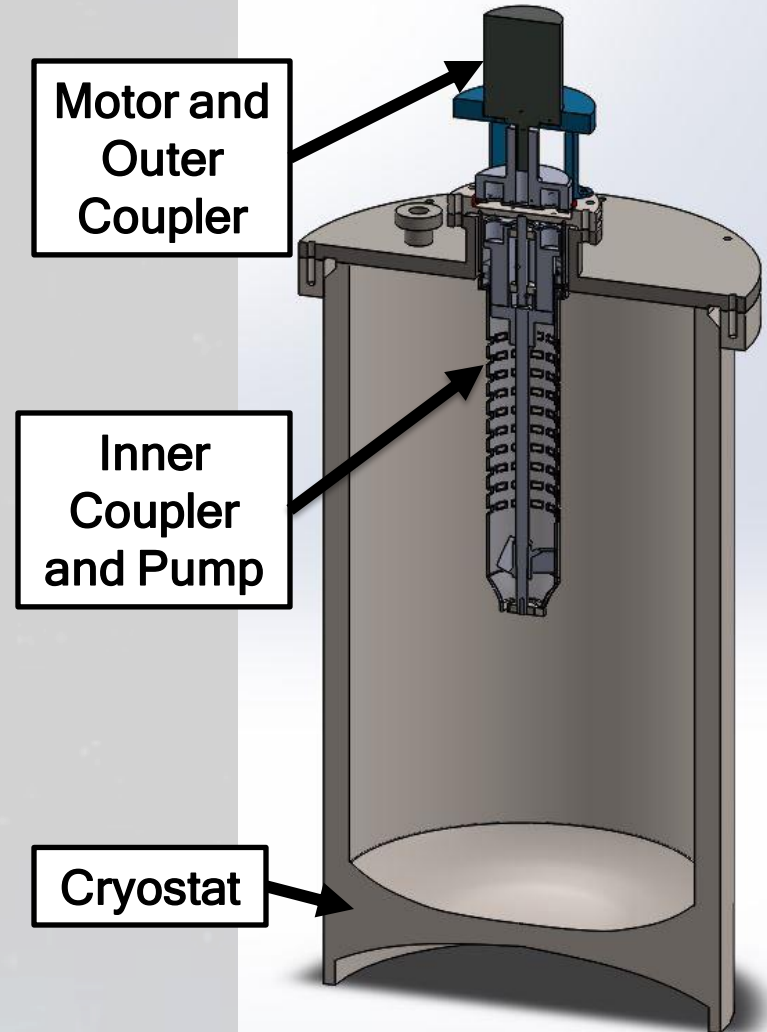
# Project Description



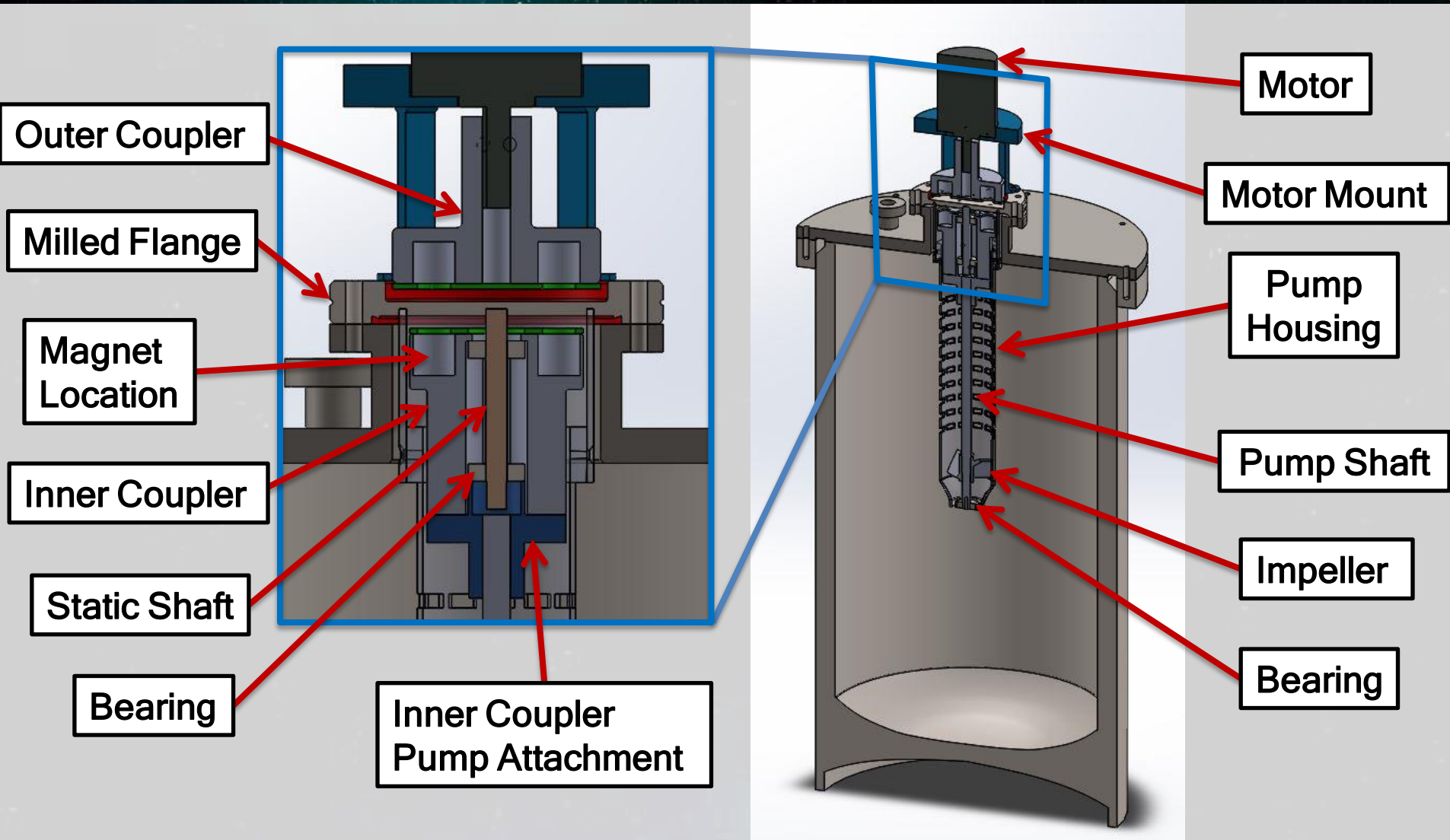
- Design an electric motor-pump/mixer unit that makes use of magnetic coupling technology.
  - The motor must be on the outside of the cryogenic tank
  - Meets volumetric flow rate of current system (5-15 gpm)
  - The entire pump system must fit through a 3.75 inch port on top of the tank

# Prototype Design

- Suspension
  - Bearing System at static shaft and pump housing
- Magnetic Coupling
  - Four 0.75" diameter 1 T magnets coupled through milled flange to paired four
  - Distance between the couplers 0.75 in
- Motor
  - Provides sufficient power to mix 5-15 gpm
- Size Constraints
  - Coupler and Pump System fit through 3.75" port

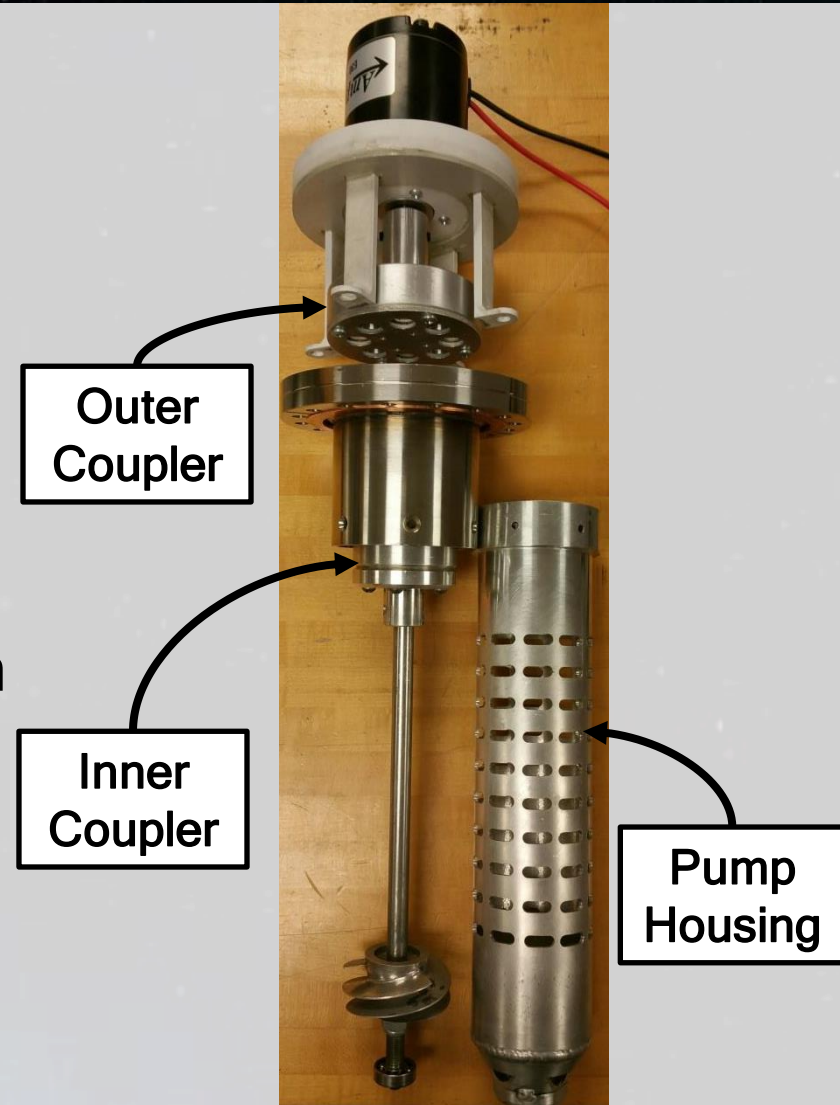


# Prototype Design



# Design Assembly

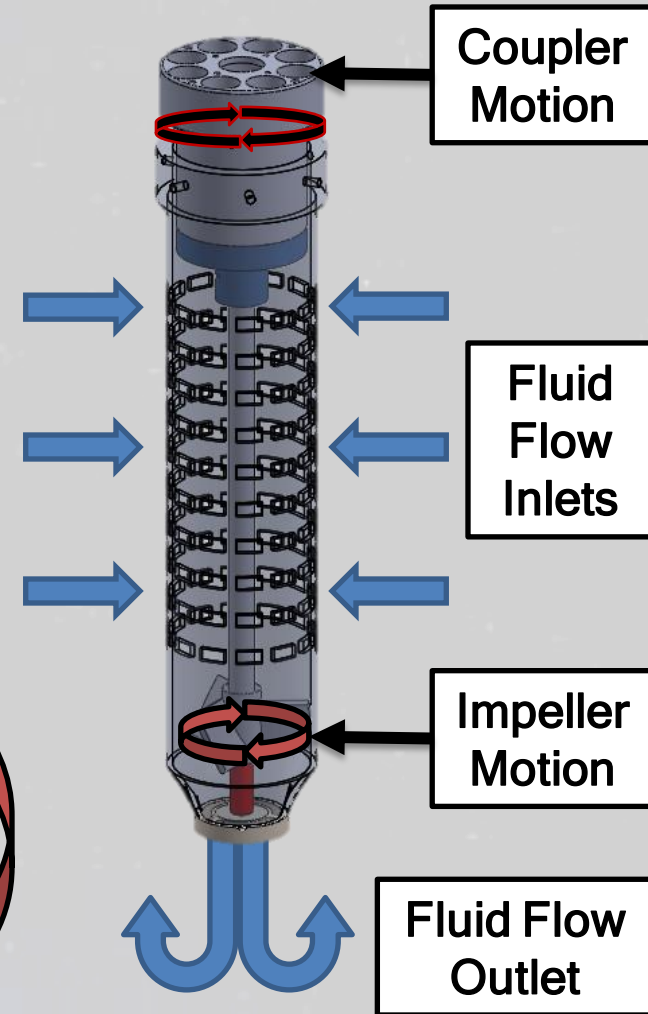
- Outer coupler secured to motor right above flange
- Weld static shaft and pump anchor and bearing plate
- Attach fully assembled Inner Coupler
- Press fit bearings and bushing
- Connect Pump Attachment with attached Pump Shaft and Impeller
- Assemble Pump Housing over Pump Shaft (press fit end bearing)





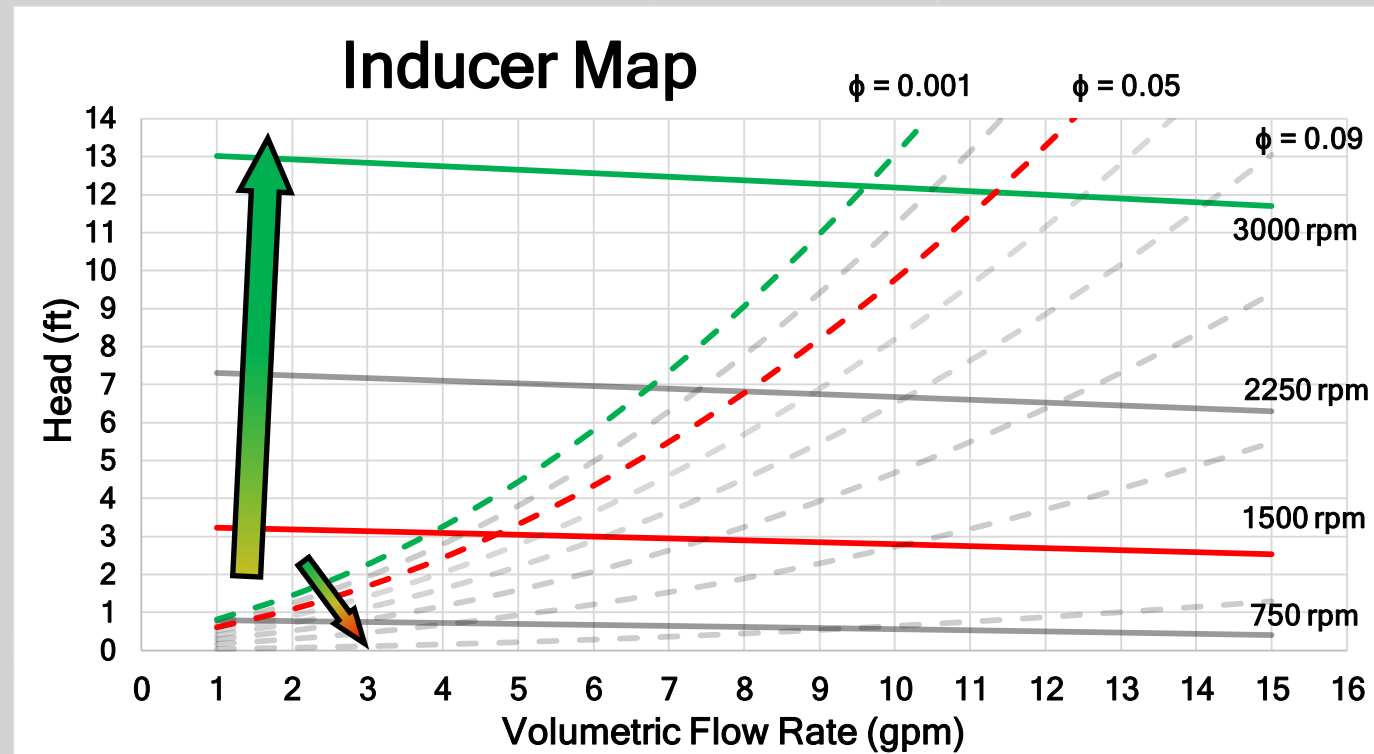
# Pump Design

- Rotational motion from the inner coupler (black arrows) spins impeller (red arrows)
- Impeller motion sucks fluid from inlets through pump housing and through outlet
- Inlets begin 3" from top of tank to ensure suction
- Outlet located 13" inside tank as per sponsor specification



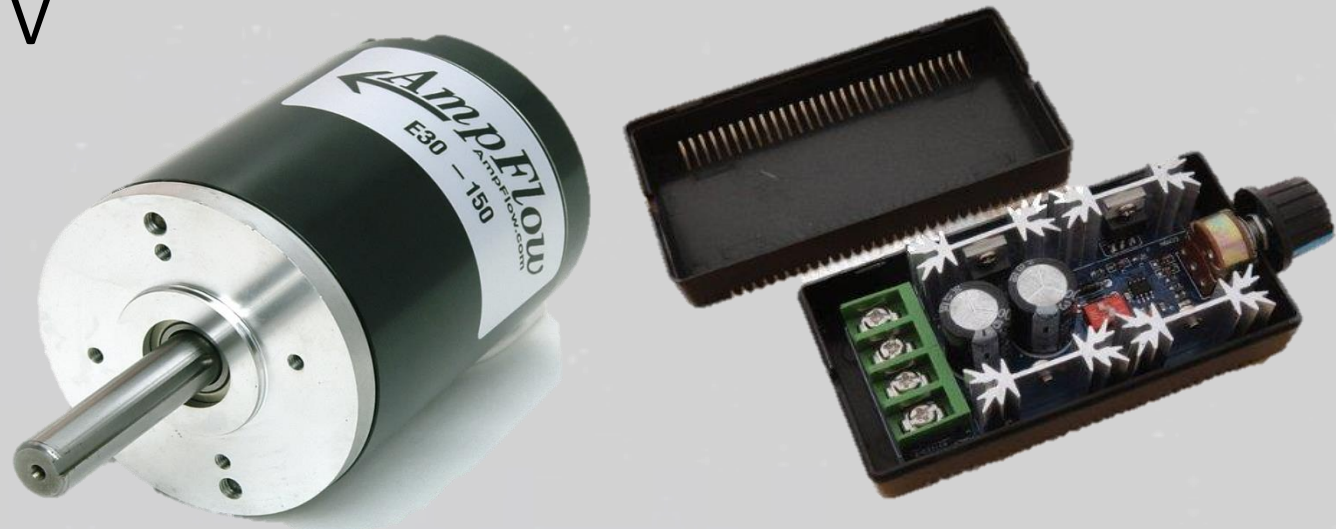
# Pumping Capacity Analysis

- Head needed found to be 3 ft.
- Needed power of motor found to be  $>0.5$  HP.
- Pumping calculations using non-dimensionalized flow coefficient ( $\phi$ ) and RPM.
- Lower flow coefficient,  $\phi$ , wanted.
- Motor needs to output  $>2500$  RPM.



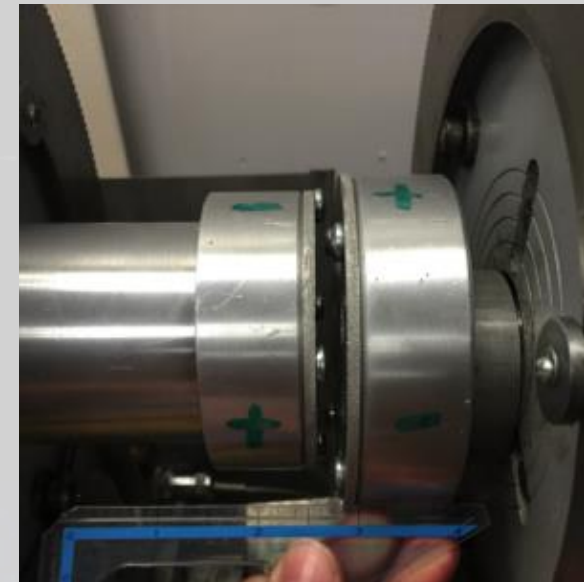
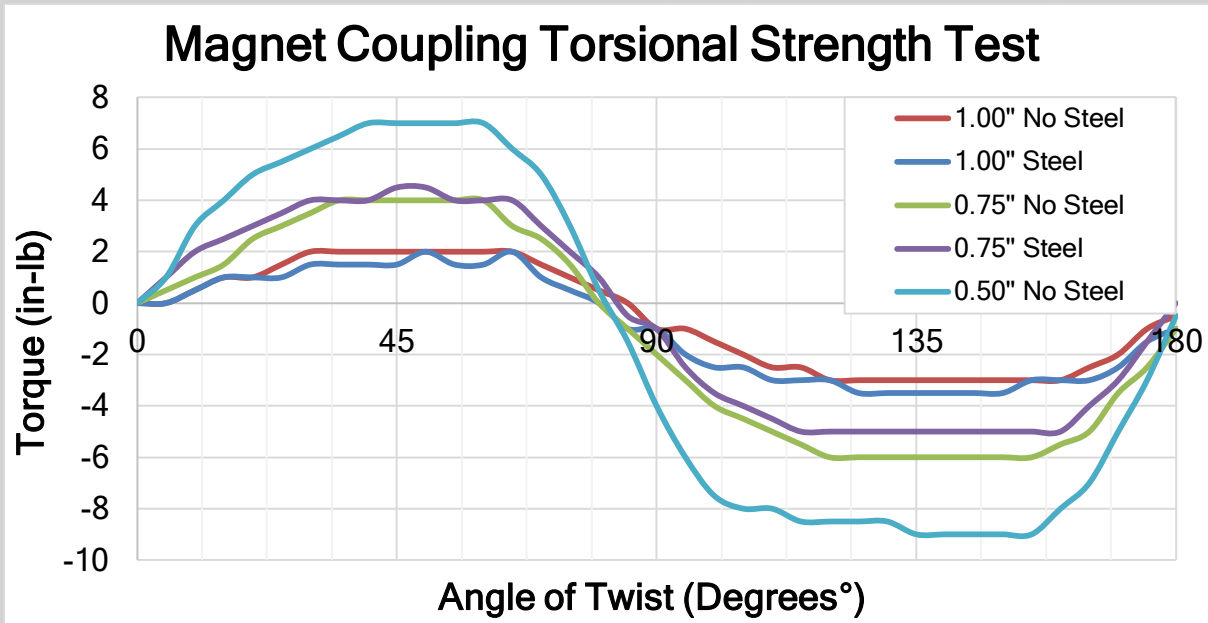
# Motor Specification Analysis

- Motor purchased 24 V DC motor that provides a Peak HP of 1.0 and an RPM @24V of 5600.
- Motor controller using a potentiometer used to control motor speed.
- Using one 24 V DC battery provided to the group by Dr. Gupta



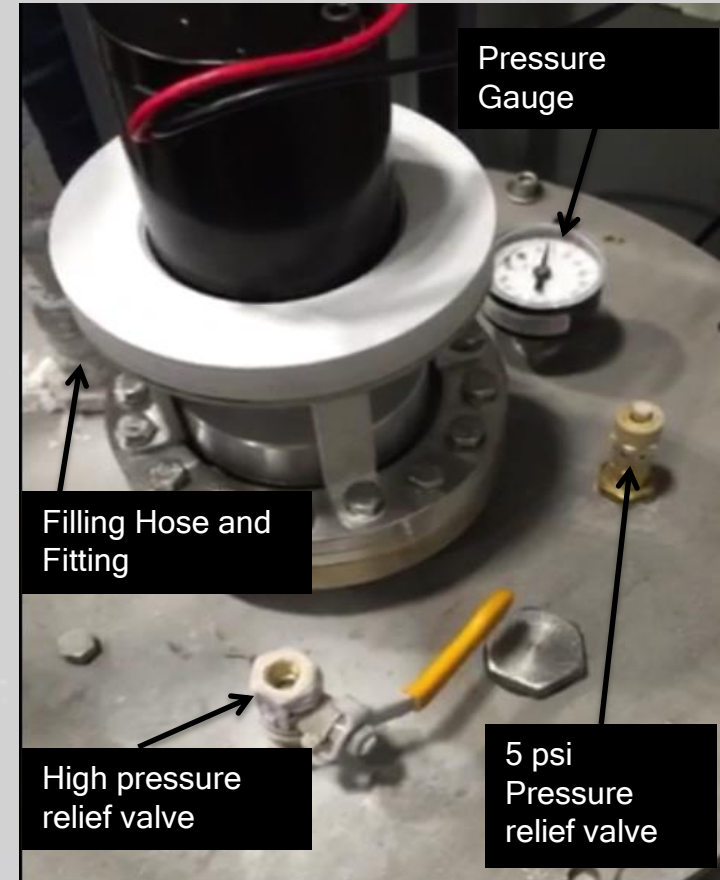
# Magnet Experimental Analysis

- Magnet number reduced from 8 to 4
- Reduction amplifies coupling strength
- Tested at 1.0", 0.75", and 0.5" with and without steel plate
- Rotates at 20°/min with recordings every 5°
- At the coupler distance, maximum torque found to be 4 in-lbs.



# Safety

- Cryogenics
  - LN temperature range: 63K – 77K
- Pressure build up
  - Pressure relief valve
  - Sealing
- High velocity components
- Electrical components
- Magnets



# Experimental Testing

- Water Testing
  - Ensure design is operable in water
- Volumetric Flow Rate
  - Design piping system
  - Connect flow meter
  - Record maximum Flow Rate



# Experimental Testing

- Liquid Nitrogen
  - Ensure design operable in liquid nitrogen
  - Recorded frequency of pressure relief
    - Without pump
    - With pump



# Water Test Results

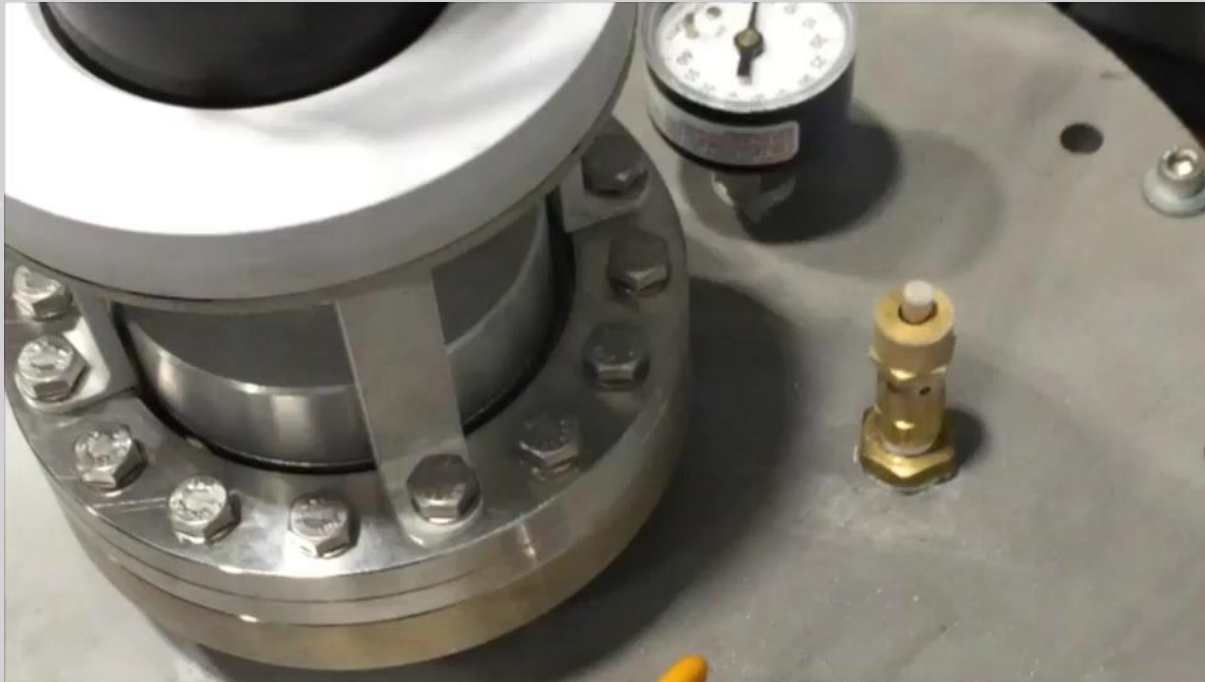
- Water Testing
  - Successful
- Volumetric Flow Rate
  - Reached an average maximum flow rate of 14gpm
  - Maximum flow rate of 16gpm





# Cryogenic Test Results

- Liquid Nitrogen Testing
  - Without pump frequency of 0.6Hz
  - With pump frequency of 0.3Hz

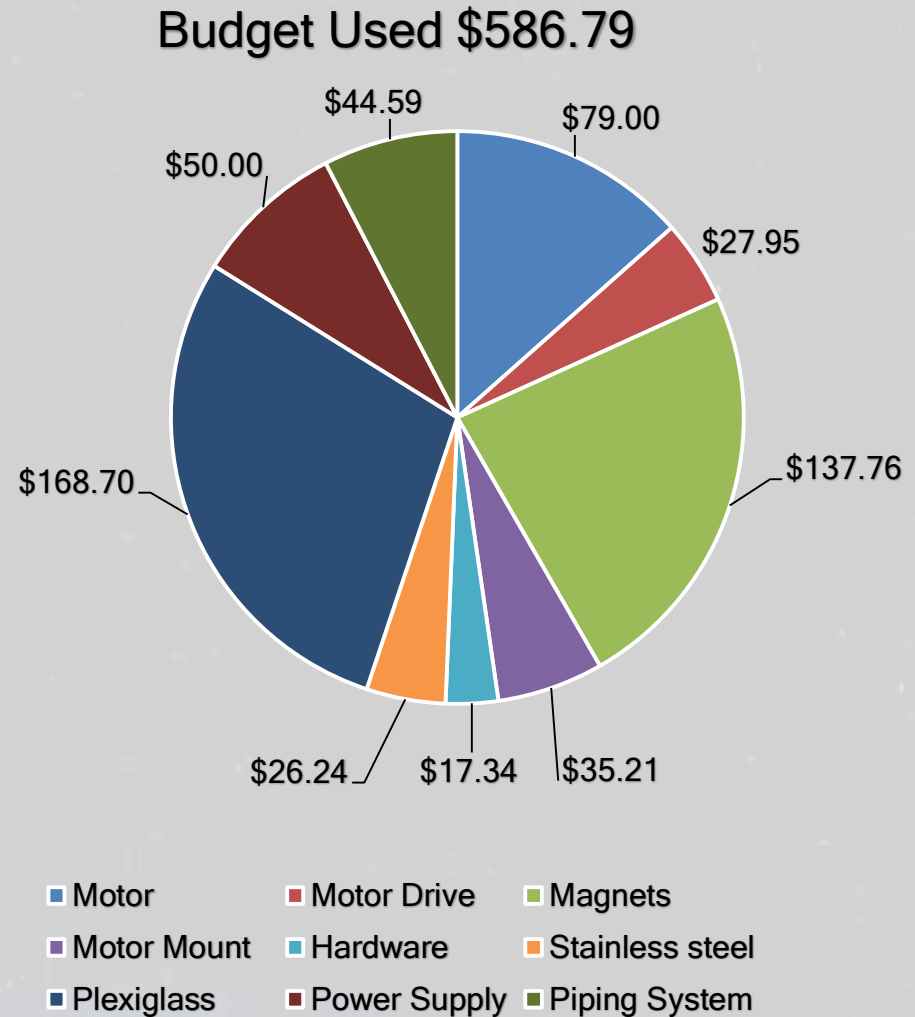


# Reliability

- Bearings
  - Life of 8000hrs
- Magnets
  - Minute decrease in strength over 10 years
  - High strength in cryogenic temperatures
- Materials
  - High strength
  - No ductile to brittle transition

# Budget and Procurement

- Budget \$600 Florida Space Grant
- Materials Purchased
  - Bearings
  - Magnets
  - Motor
  - Motor Driver
  - Plexiglass
  - Nuts & Bolts
- Materials Supplied
  - Fabrication Materials
    - Aluminum
    - Stainless Steel
  - Cryofab CF 1424-F
  - 6" ConFlat SS flange
  - Impeller



# Scheduling



# Future Improvements

- Bearings
  - Incorporate dry lubricant
- Vibration Analysis
  - Motor mount
  - Pump shaft
- Nonmagnetic materials
- In depth prototype testing

# Conclusion

- Design an electric motor-pump/mixer unit that makes use of magnetic coupling technology.
- Magnet number reduced from 8 to 4
  - Produced 4 in-lbs of torque
- Volumetric Flow Rate
  - Reached an average flow rate of 14gpm
  - Maximum flow rate of 16gpm
- Cryogenic Testing
  - Reduced venting by 50%

# References

- [1] Senior Design Project Definition Group 24. N.p.: n.p., n.d. PDF.
- [2] W., Van Sciver Steven. Helium Cryogenics. New York: Plenum, 1986. Print.
- [3] "Magnetic Couplings | Technology | Magnomatics." Magnetic Couplings | Technology | Magnomatics. N.p., n.d. Web. 25 Sept. 2014.
- [4] "HowStuffWorks "Parts of the Tesla Turbine"" *HowStuffWorks*. N.p., n.d. Web. 09 Oct. 2014.
- [5] Pump, Nikkiso Cryogenic. *NIKKISO CRYOGENIC PUMP* (n.d.): n. pag. Web.

# Questions?



Website: [http://eng.fsu.edu/me/senior\\_design/2015/team24/](http://eng.fsu.edu/me/senior_design/2015/team24/)

Group 24  
Janet Massengale



# Project Specifications

Requirement	Specification
Tank Size	<ul style="list-style-type: none"><li>• Height: 29 in</li><li>• Outer Diameter: 16 in</li><li>• Inner Diameter: 14 in</li><li>• Gross Capacity: 60 Liters</li></ul>
Insulation	<ul style="list-style-type: none"><li>• 0.5 in of foam</li><li>• &gt;20 layers of multi-layer insulation (MLI)</li></ul>
Mounting	<ul style="list-style-type: none"><li>• Mounted to 6 in flange</li><li>• Flange has 4 in port into tank</li></ul>
Pump Motor	<ul style="list-style-type: none"><li>• Variable Flow Rate : 5 - 15 gpm</li><li>• Generates 5 psid rise in pressure</li><li>• Mixer/Pump must reach 12 inches into tank</li></ul>
Additional Requirements	<ul style="list-style-type: none"><li>• Tank must be adiabatic to surroundings</li><li>• Pump shaft must be magnetically coupled to the motor shaft</li><li>• Friction must be held to a minimum</li><li>• System must be compact</li><li>• Materials used for the magnetic housing and flange must be non magnetic</li><li>• Materials must withstand extremely cold temperatures between 63K - 77.2K</li></ul>

# Bill of Materials

Part	Vendor	Purpose	Quantity	Cost per Item	Total Cost
Magnets	K&J Magnets	Magnetic coupling	16	\$8.61	\$137.76
Motor	Amazon	Motor	1	\$79.00	\$79.00
Motor Drive	Amazon	Control Motor Speed	1	\$27.95	\$27.95
PVC 12"x12"x 1"	Amazon	Motor Mount	1	\$35.21	\$35.21
6-32 x 1/2"	Fastenal	Assembly	10	\$0.20	\$2.00
10-32x1/2"	Fastenal	Assembly	10	\$0.20	\$2.00
10-32x3/4"	Fastenal	Assembly	5	\$0.40	\$2.00
10-32 Nyloknut	Fastenal	Assembly	10	\$0.30	\$3.00
1/4-20x3/8"	Fastenal	Assembly	10	\$0.30	\$3.00
8-32X1.5"	Fastenal	Assembly	5	\$0.40	\$2.00
Keystock 1/8"x1/8"x1'	Fastenal	Assembly	1	\$0.65	\$0.65
3/16x1.25" clevis pin	Fastenal	Assembly	1	\$0.23	\$0.23
3/16x7/8" clevis pin	Fastenal	Assembly	1	\$0.24	\$0.24
3/16X3/4" clevis pin	Fastenal	Assembly	1	\$0.20	\$0.20
Cotter pin 1/16 x1	Fastenal	Assembly	20	\$0.10	\$2.00
12v Battery	FourAcre	Power supply	1	\$50.00	\$50.00
Stainless Steel	Online Metals	Pump Anchor	1	\$26.24	\$26.24
				<b>Design Cost</b>	<b>\$373.48</b>
12"x24"x.5" Plexiglas	Professional Plastics	Testing Tank	4	\$35.80	\$143.20
12"x12"x.5" Plexiglas	Professional Plastics	Testing Tank	1	\$25.50	\$25.50
1"x1" PVC Pipe	Home Depot	Testing system	2	\$2.23	\$4.46
1"x2" PVC Pipe	Home Depot	Testing system	2	\$3.36	\$6.72
2" 180deg Bend PVC	Home Depot	Testing system	2	\$3.23	\$6.46
PVC glue	Home Depot	Testing system	1	\$8.26	\$8.26
Silicon sealant	Home Depot	Testing system	2	\$6.75	\$13.50
Rubber PVC Reducer	Home Depot	Testing system	1	\$3.63	\$3.63
2" to 1" PVC reducer	Home Depot	Testing system	1	\$1.56	\$1.56
				<b>Testing Cost</b>	<b>\$213.29</b>
				<b>Total Cost</b>	<b>\$586.77</b>

# Bearing Calculations

$$F_r := 61\text{bf}$$

$$F_a := 10.51\text{bf}$$

$$L_h := 8000\text{hr}$$

$$\omega := 1500\text{rpm}$$

$$F_e := (F_r^2 + F_a^2)^{\frac{1}{2}} = 53.794\text{ N}$$

$$C_{-} := F_e \cdot L_{10}^{\frac{1}{3}} = 482.146\text{ N}$$

From SKF bearing catalog

$$C_0 := 193\text{N} = 43.388\text{bf}$$

From Table 11-24

$$\frac{F_a}{C_0} = 0.242$$

Linear Interpolation

$$e_{-} := .34 + (.38 - .34) \cdot \frac{.242 - .17}{.28 - .17} = 0.366$$

$$V := 1.2$$

$$\frac{F_a}{V \cdot F_r} = 1.458$$

$$Y := 1.15 + (1.31 - 1.15) \cdot \frac{.242 - .17}{.28 - .17} = 1.255$$

$$X := .56$$

$$F_e := X \cdot V \cdot F_r + Y \cdot F_a = 76.539\text{ N}$$

$$C_{-} := F_e \cdot L_{10}^{\frac{1}{3}} = 686.004\text{ N}$$

Repeat process Until C does not change

# Power Calculations

## Pumping Requirement Calculations

Given - Volumetric Flow Rate  $(V = 15 \frac{\text{gal}}{\text{min}})$

$$\text{RPM} = 1500 \frac{\text{rev}}{\text{min}}$$

$$\text{Inducer } d = 2.75 \text{ in}$$

Convert vol flow rate to  $\text{ft}^3/\text{sec}$

$$V = 0.0334 \frac{\text{ft}^3}{\text{sec}}$$

Find inducer inlet cross-sectional area

$$A = \pi \left( \frac{d}{2} \right)^2$$

$$A = 0.0412 \text{ ft}^2$$

The meridional flow velocity

$$C = \frac{V}{A}$$

$$C = 0.8102 \frac{\text{ft}}{\text{sec}}$$

The tip speed is then found

$$U = \frac{\text{RPM} \cdot d}{2}$$

$$U = 17.9987 \frac{\text{ft}}{\text{s}}$$

The flow coefficient is found

$$\phi = \frac{C}{U}$$

$$\phi = 0.045$$

From the given plot, the head coefficient is found

$$\psi = \left( -4.0168 \cdot \phi^2 \right) - (1.4598 \cdot \phi) + 0.3254$$

$$\psi = 0.2515$$

The head of the pump is then found

$$\text{Head} = \frac{\psi \cdot U^2}{\left[ 32.174 \frac{\text{ft}}{\text{sec}^2} \right]}$$

$$\text{Head} = 2.5328 \text{ ft}$$

Convert the volumetric flow rate converted into mass flow rate

$$m = V \cdot 62.3 \frac{\text{lb}_f}{\text{ft}^3}$$

$$m = 2.0821 \frac{\text{lb}_f}{\text{s}}$$

Power requirement assuming 20% efficiency

$$P = \frac{m \cdot \text{Head}}{0.2}$$

$$P = 0.0479 \text{ hp}$$

With a factor of safety of x5 to x10

$$\text{Power} = 10 \cdot P$$

$$\text{Power} = 0.4794 \text{ hp}$$