

#20 - Direct Drive Solar Powered Arcjet Thruster

SPONSOR – NASA, MARSHALL SPACE FLIGHT CENTER, HUNTSVILLE AL

ADVISORS – DR. GUO, DR. KWAN, DR. ANDREI

SENIOR DESIGN COORDINATORS – DR. AMIN, DR. FRANK



Team Members

Date – 3/18/14

Chris Brolin - ME

Cory Gainus - ME

Gerard Melanson - ECE

Tara Newton - ME

Griffin Valentich - ME

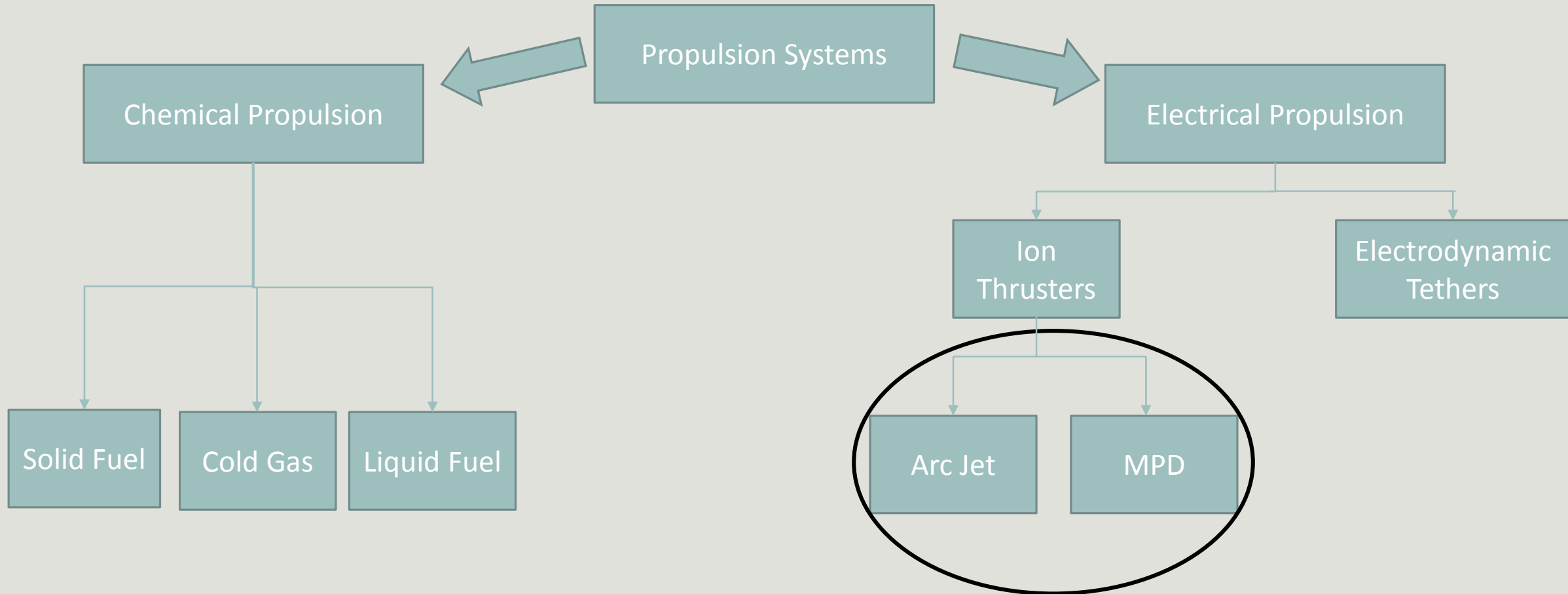
Shane Warner - ECE

Griffin Valentich

Agenda

- Background
- Sponsor Requirements/Objectives
- Final Design
 - Mechanical
 - Electrical
- Testing Overview
- Procurement
- Future Plans
- Gantt Chart

Background



Background

- Electrical Propulsion Systems
 - High specific impulse – low thrust
 - Electro-thermal thruster– arcjet
 - Produce thrust by heating gas propellant (Ar) and expelling through C-D Nozzle
 - Electromagnetic thruster – MPD
 - Accelerates particles with applied magnetic force
- Purpose of Electric Propulsion Systems
 - Station keeping – lower overall lifetime costs
 - Satellite altitude and attitude adjustment
 - Potential for deep space applications
- Power Processing Unit (PPU)
 - Expensive and complex
 - Largest prohibitive component to electronic propulsion systems
 - Converts input power to correct current and voltage

Sponsor Requirements / Objectives

- **Eliminate the PPU**

- Enable thruster to operate in Direct-Drive Mode
- Obtain power directly from solar panels

- **Design, manufacture, and test an arcjet thruster**

- Utilize permanent magnets to confine focus ion stream to increase thrust
- Independently control propellant flow
- Design mounting apparatus and a workable vacuum chamber
- Measure thrust produced

- **Quantify the range of operating conditions over which thruster is effective at operating continuously**

Paschen's Law

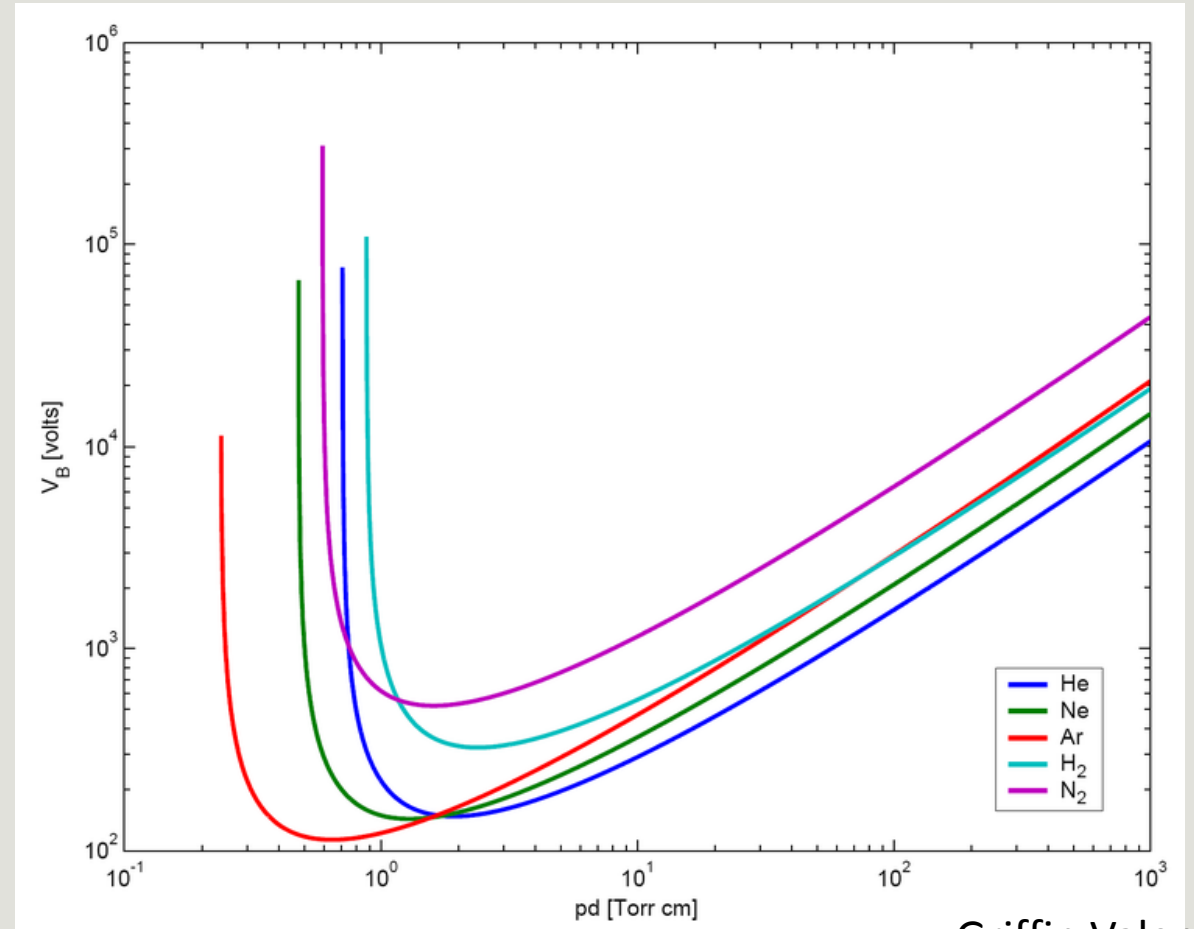
- Relates the product of pressure and distance between anode and cathode to the voltage necessary to initiate breakdown

$$V_{Breakdown} = f(P * d)$$

- Argon had lowest breakdown voltage

$$\sim 137 V$$

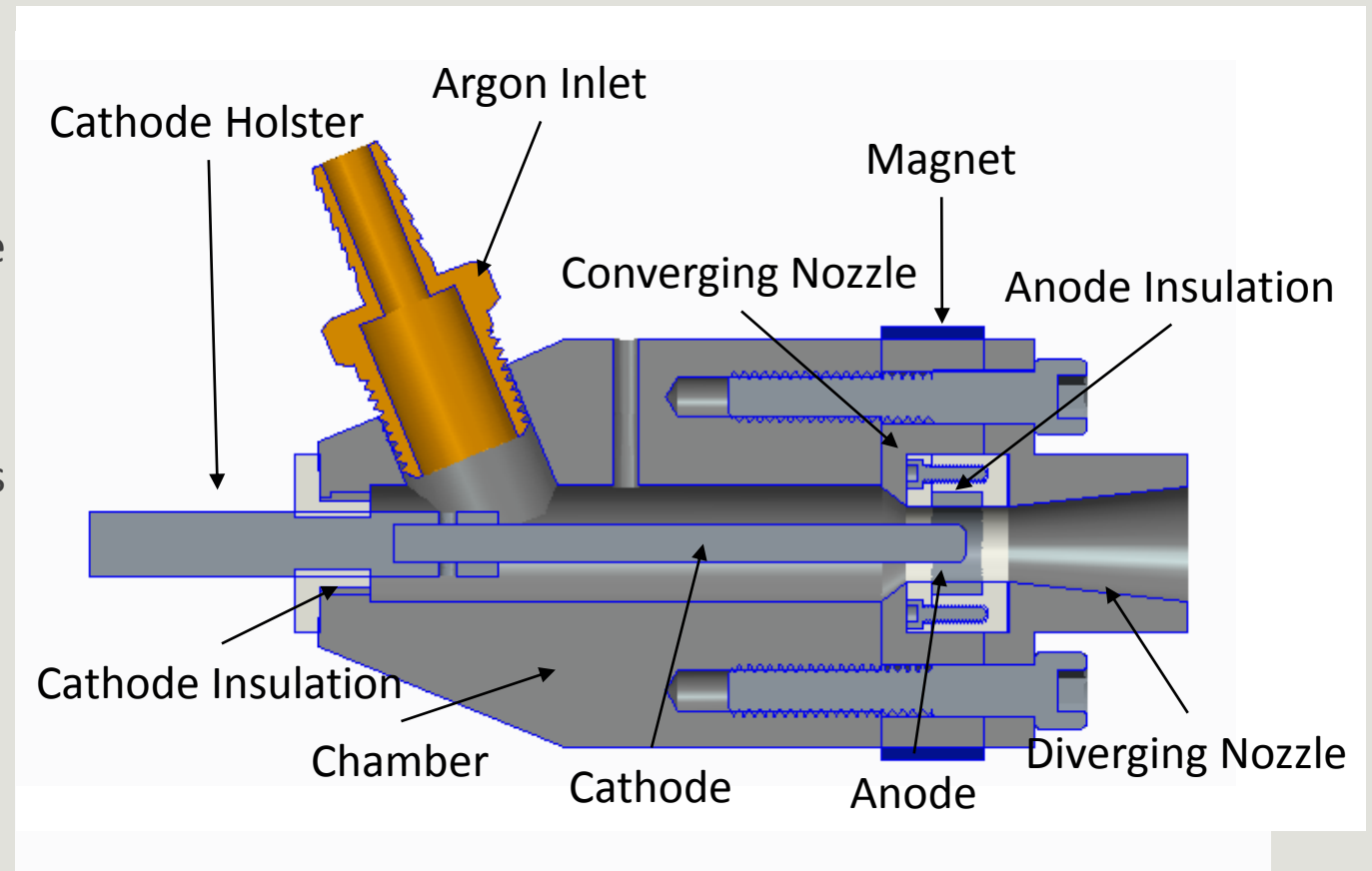
- Good starting point, but values will be different due to complex geometry



Final Thruster Design

Characteristics

- 3 part nozzle construction
 - Easier machinability
 - Designed for Mach 2.65 - $A/A^* = 3.15$
- Magnet placed at throat of nozzle to protect nozzle walls
- Stagnation Pressure – 550 Pa
- Static Pressure at throat – 267 Pa
 - Pressures from Bernoulli's Eq with const. mass flow rate
 - $P/P_0 = 0.4867$, at throat $M = 1$
- Anode/Cathode Spacing – 0.15"
- Product of pressure and distance gives breakdown voltage of 137 V
 - Well within circuit's capabilities



Testing Apparatus

Vacuum Pump

- Welch 1400
- Vacuum to 1×10^{-4} Torr



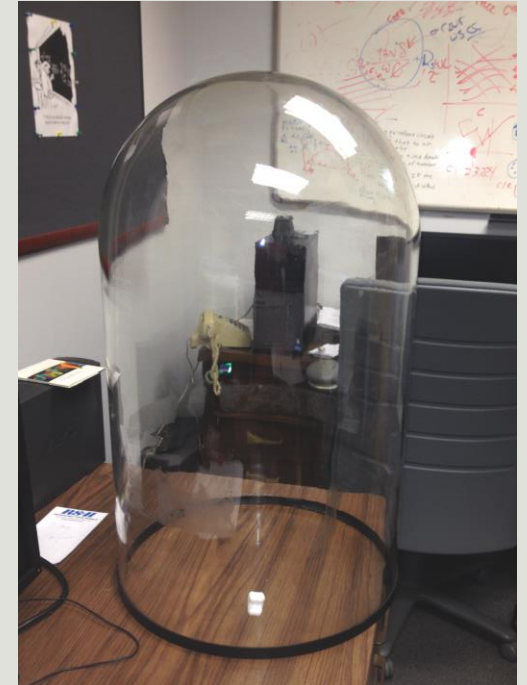
Baseplate

- Borrowed from Dr. Weatherspoon
- Argon and electrical connection input through baseplate



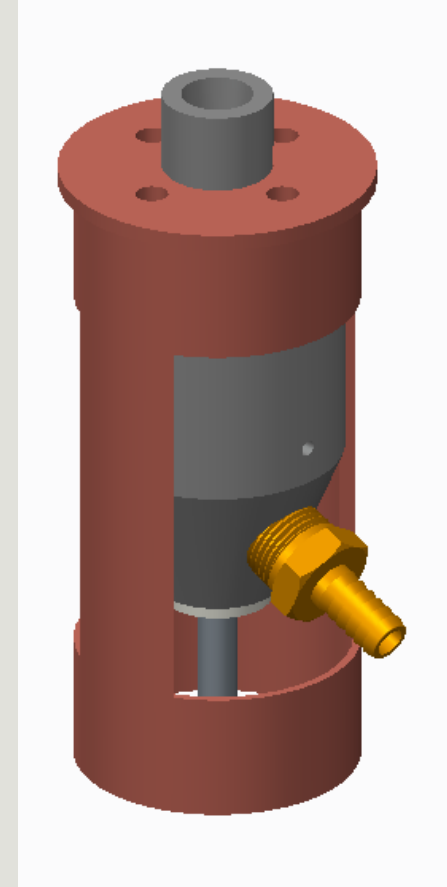
Vacuum Chamber

- Bell Jar
- Borrowed from Dr. Weatherspoon
- Chamber will be evacuated to 1×10^{-4} Torr



Test Stand

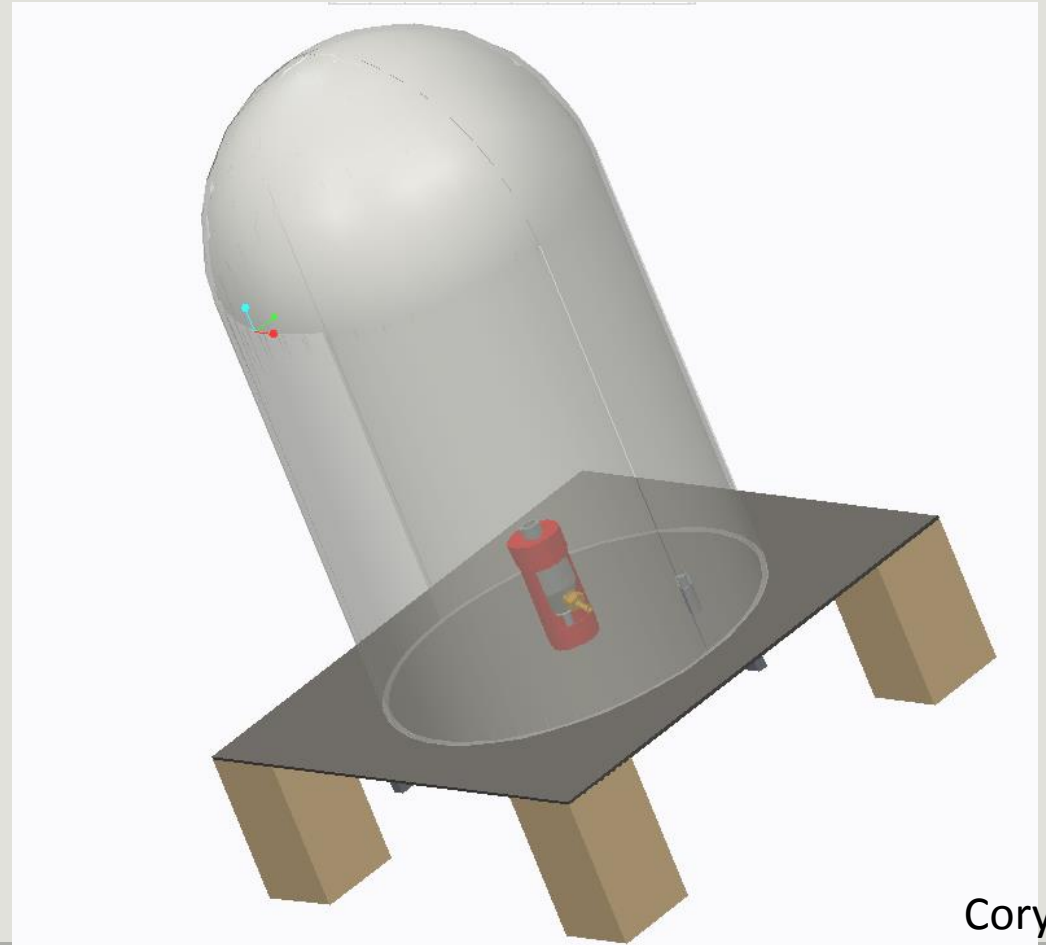
- Standard Pipe with cap
 - Separate Pieces
- Easy to machine
- Easily attached to thruster and detached for any required adjustments
- Lightweight
- Easy to access argon and pressure ports
- Adaptable for whatever force measurement equipment is used



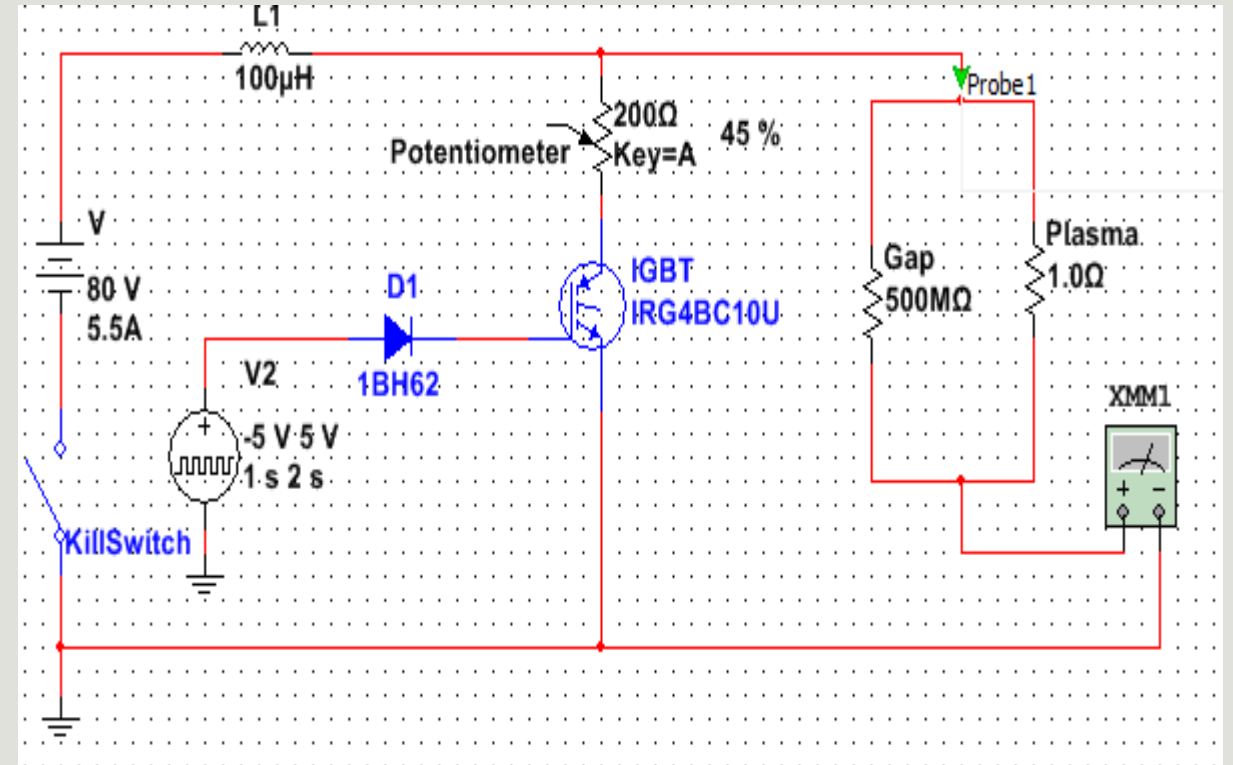
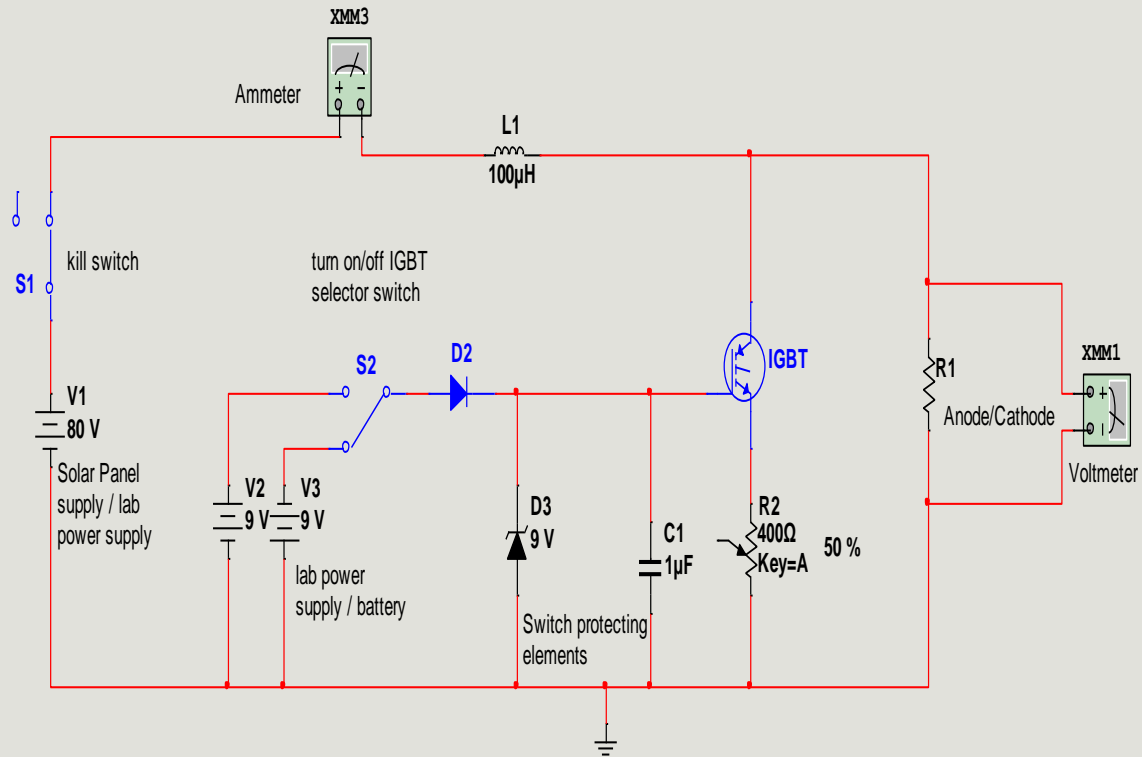
Cory Gainus

Final Testing Set Up

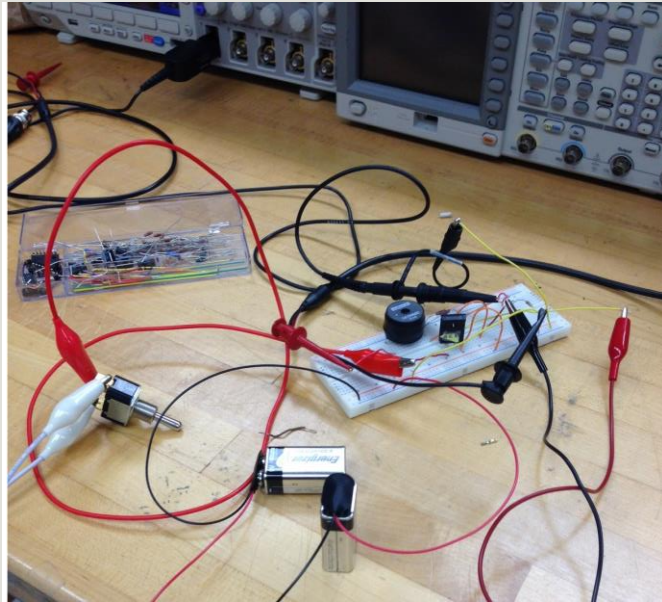
- Square steel tubing reinforced baseplate
- Pipes welded for
 - Vacuum hose
 - Vacuum gauge
 - Argon inlet
- Wires throughput with stycast epoxy
 - Supplied by Dr. Guo
- Edges of chamber sealed with vacuum grease



Circuit Alterations



Testing and Results



Full Circuit Testing

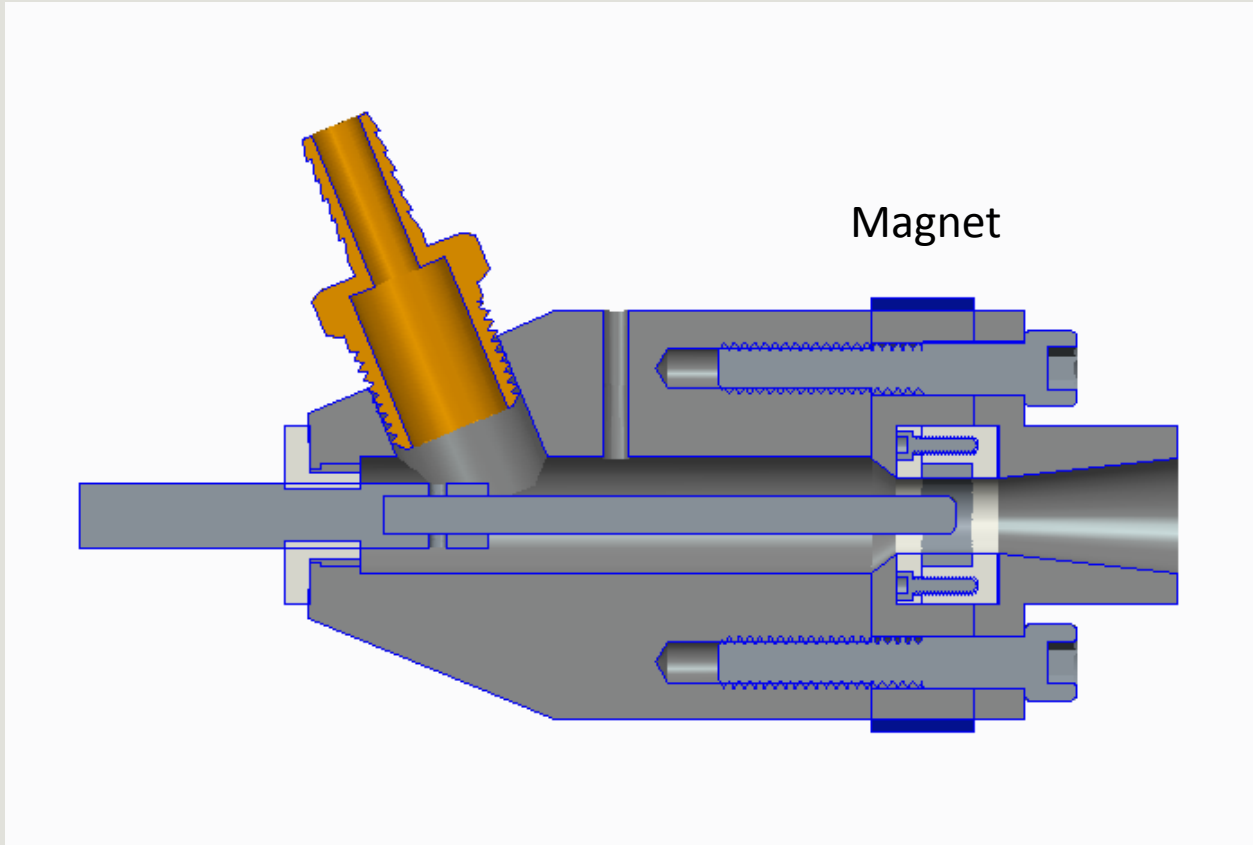
Approximately
150 V spike at
 $V_{source} = 20\text{ V}$
and
 $R_{top} = 50\text{ ohm}$



Theoretical max spike
2 kV

Gerard Melanson

Final Magnet Design



$$B = \mu_r \mu_0 \frac{N}{L} I$$

B = Magnetic field strength

μ_r = relative permeability

μ_0 = free space permeability

N = number of turns

L = Length of electromagnet

I = Current

Maximum Magnetic Field

The desired magnetic field is given by $B = \frac{mv}{qr}$, $v = \sqrt{\frac{20eV}{3m}}$, where m is mass, v is velocity, q is charge, r is radius, eV is an electron-voltage, and B is the magnetic field. These equations simplify to give us

$$B = 0.316 \text{ T}$$

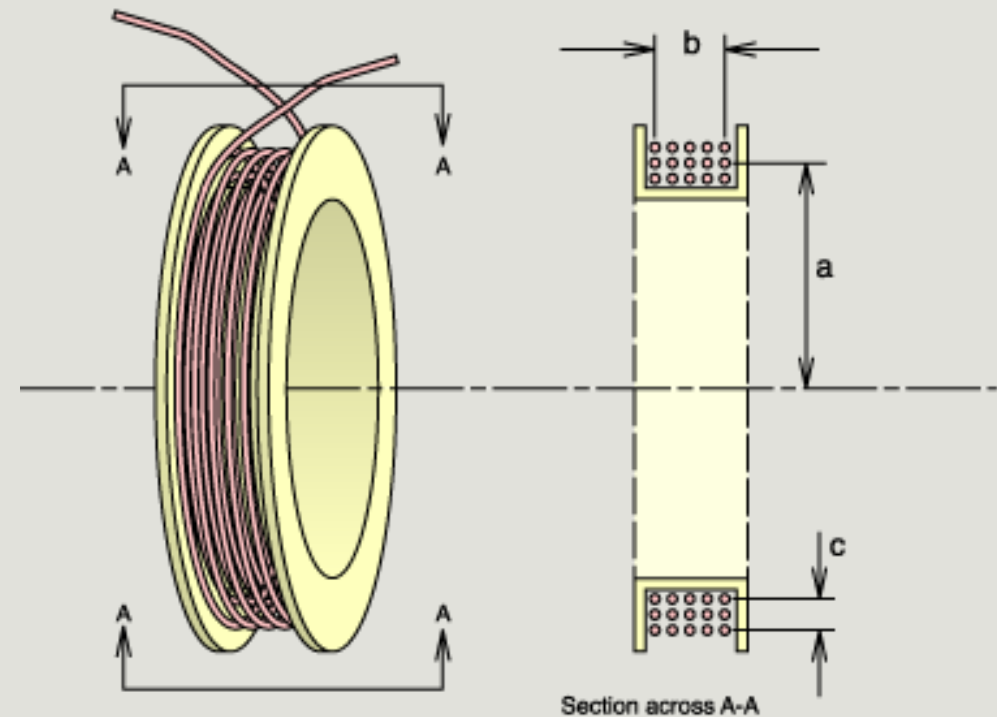
Now the current and number of turns we need is given by:

$$NI = \frac{LB}{\mu_r \mu_0} = 4790 \text{ (A - turns)}$$

Magnet Design

Max Current = 5 A
Length = 0.01905 m
Diameter of 22 gauge wire = 0.0017 m
Number of loops per layer = 11
Absolute max field = 0.316 T = 4790 A-turns
Typical ideal field = 0.050 T = 758 A-turns
At least 14 layers needed
Coat with layer of insulation between wire layers

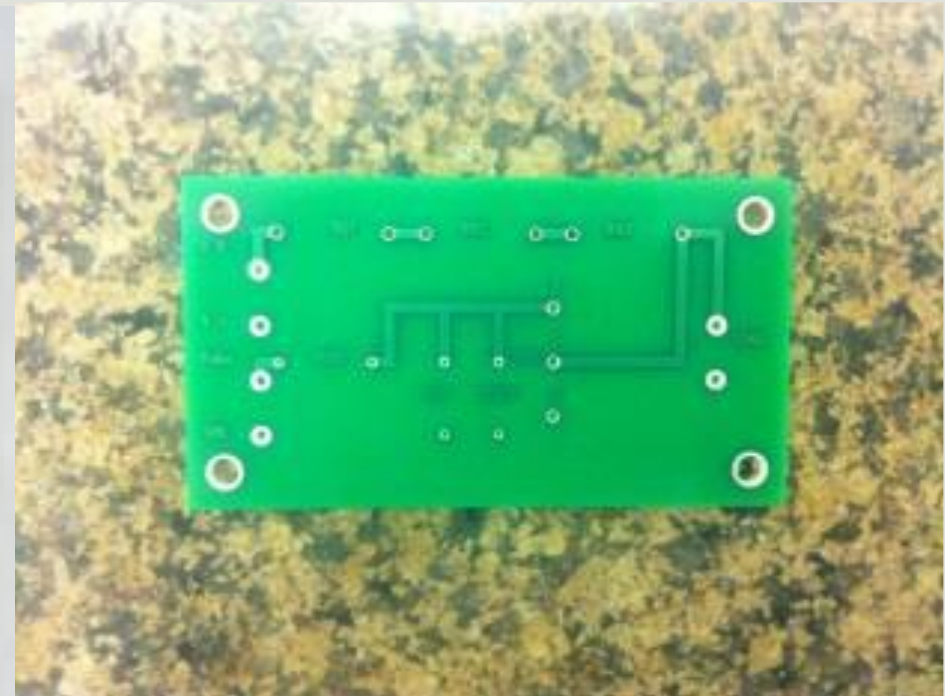
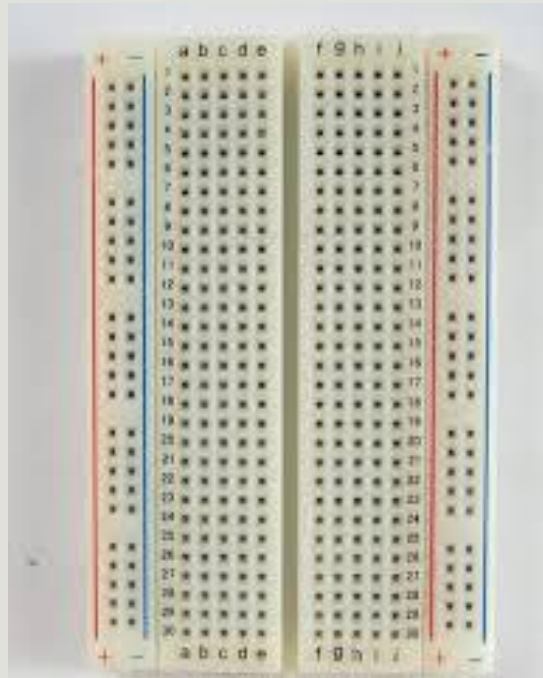
Fig. 1 Dimensions of a multi-layer coil of rectangular cross section



Gerard Melanson

Circuit Testing and Finalization

- We are currently designing the PCB on Eagle now that the design has been finalized

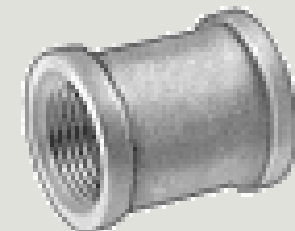
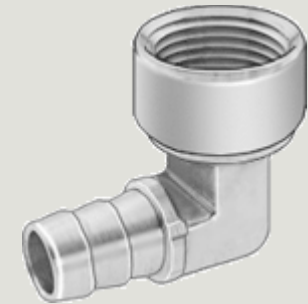
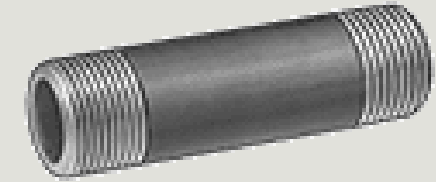


Procurement

Through baseplate hardware

Component	Part #	Quantity	Cost
Threaded Pipe Nipple	44615K462	2	\$3.24
Vacuum Hose Fitting 90 deg	5346K125	1	\$10.20
Coupling for Vacuum Gauge	4429K111	1	\$5.70
		Total	\$19.14

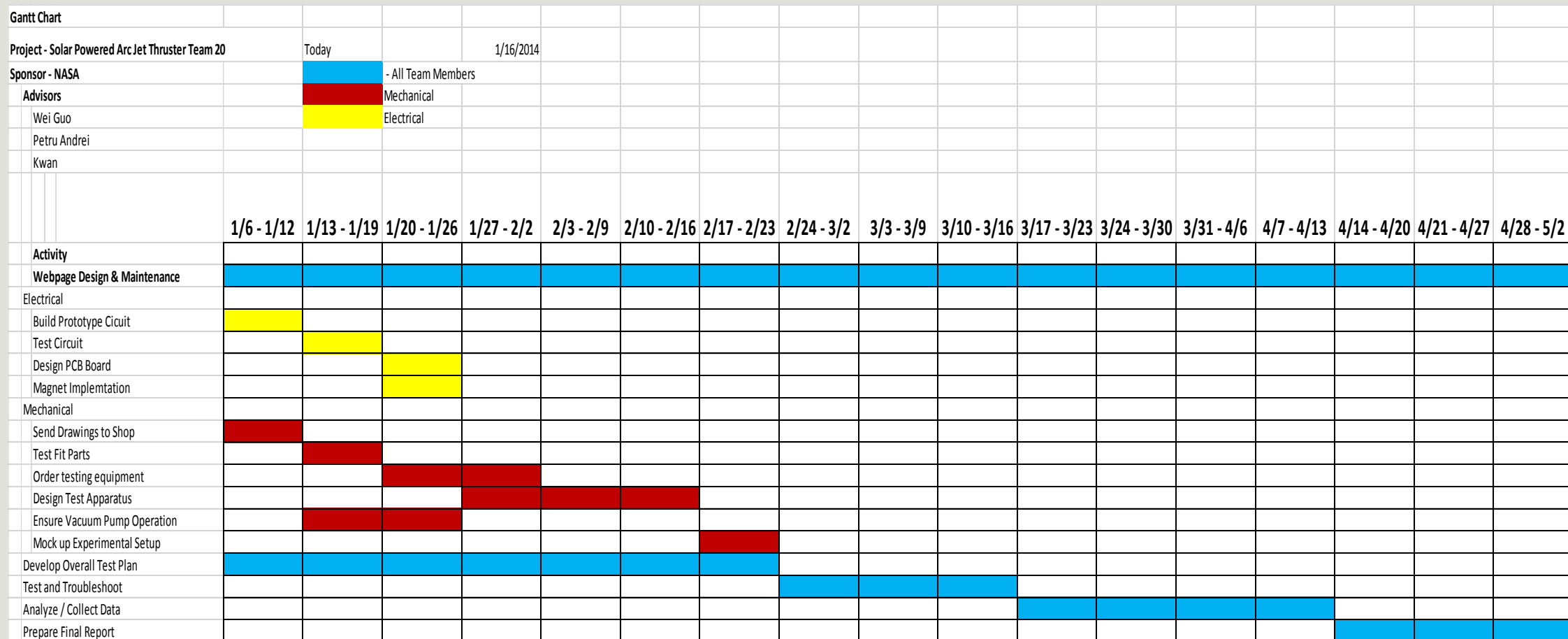
- Remaining hose fitting and poly flow hose will be supplied by sponsor
- **Remaining Budget – \$130.74**



Future Plans

- Machining baseplate
 - Mounting apparatus completed
 - Weld tubes and attach appropriate fittings
- Test vacuum chamber and leak proof connections and through holes
- Measure resistance of plasma
 - Determine whether to insert additional resistor or transconductance amplifier
- Determine thrust output and range of operating conditions
- Acquire Printed Circuit Board

Gantt Chart



Questions?
