

Bolted Joint Rig Test Development

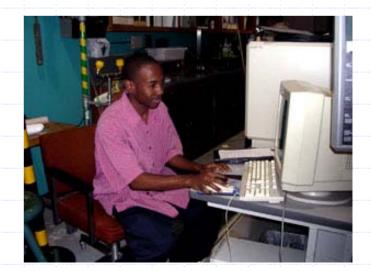
Alex V. Dugé Ana Erb Ronald Rolle Cedric White



Outline

Project Purpose
 Bolt / Metal Fatigue Overview
 Material Testing System (MTS)
 Design needs and specifications
 Design generations and selection

- Parts and cost analysis
- Testing
- Results
- Recommendations
- Conclusion

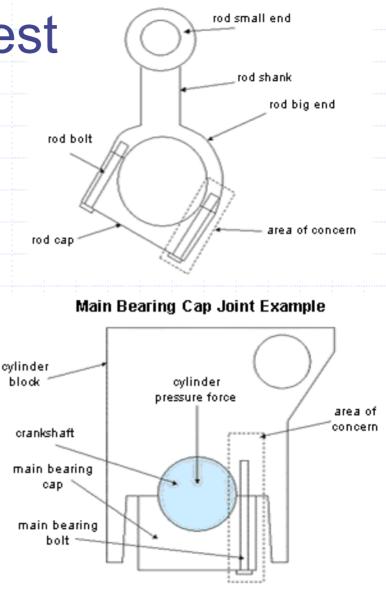


Connecting Rod Joint Example



Bolted Joint Rig Test Development

The purpose of the project is to design a test fixture that can be used to evaluate design improvements to fatigue life of threaded joints. While most of the bolt load is carried in the first few threads, this is not necessarily where failure occurs.





Project Objective

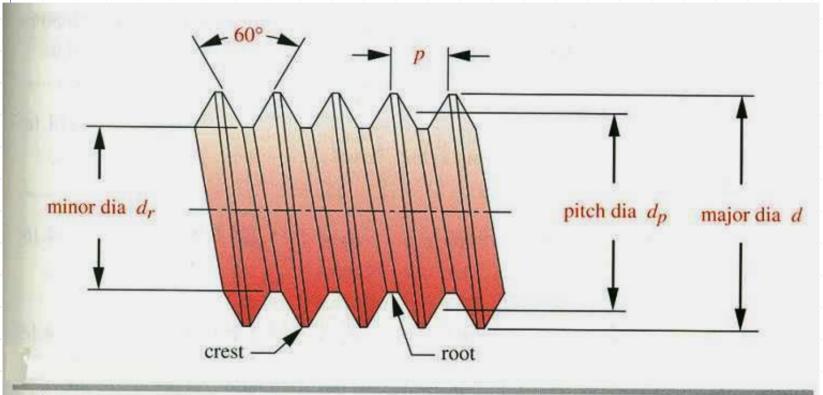
- Cummins needs
 - A test fixture than can evaluate threaded joints
 - Connecting rod
 - Main bearing cap
 - Fatigue failure on threaded joints



- Industrial needs
 - To know when the threaded joints will fail



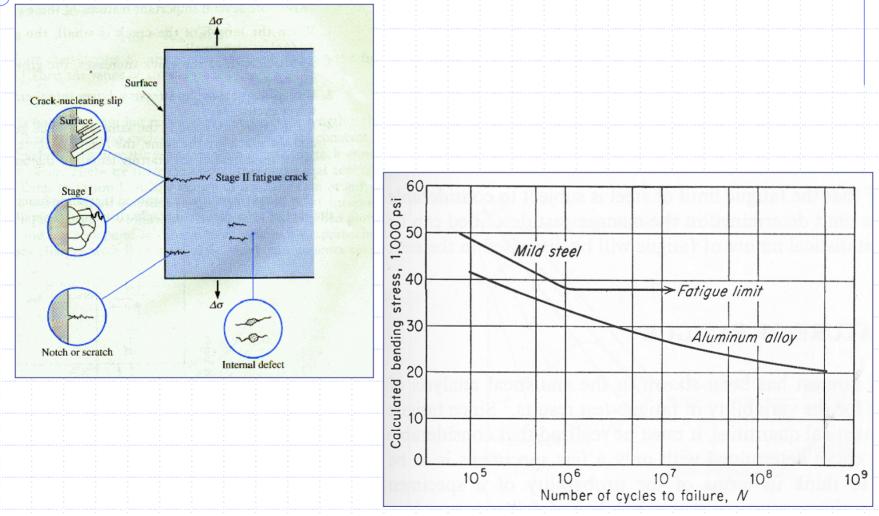
Threaded Bolt

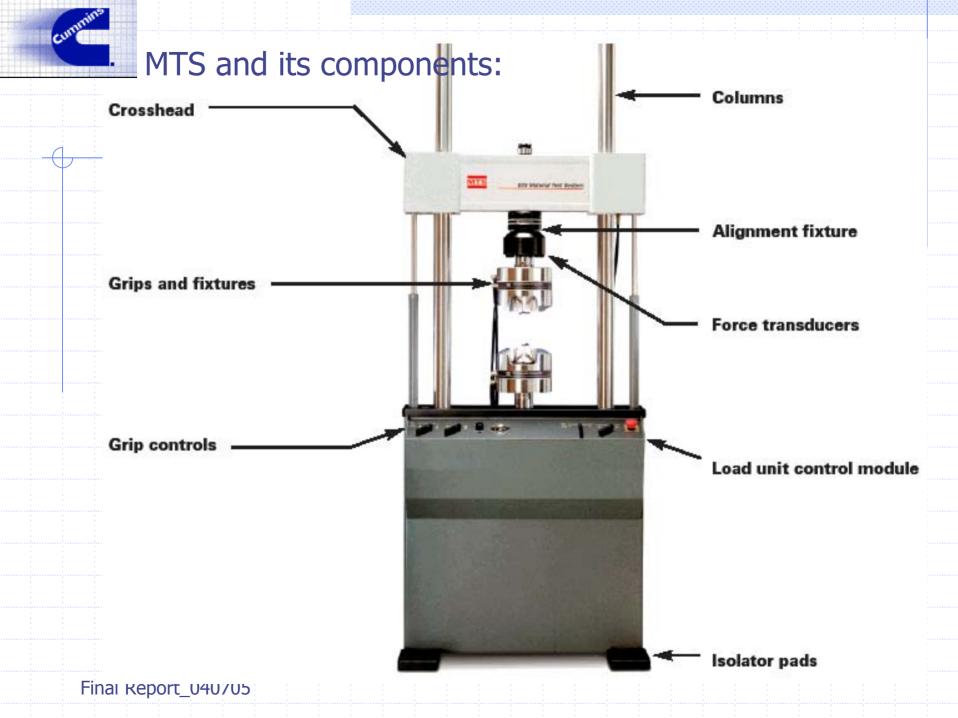


Unified National and ISO Standard Thread Form



Metal Fatigue Overview







Test Equipment

- MTS Machine
 - What it is
 - Alignment fixture
 - Grips
 - Wedges

















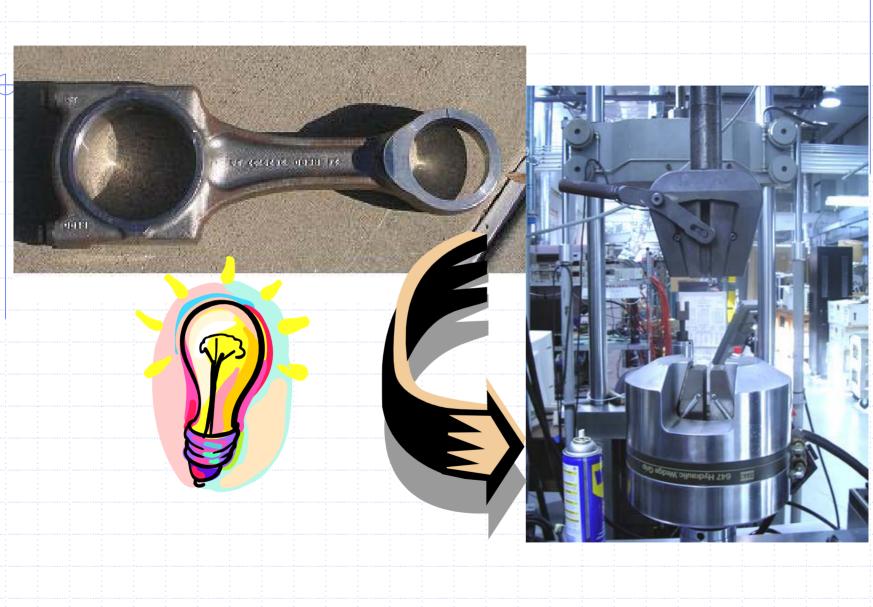
Design Needs



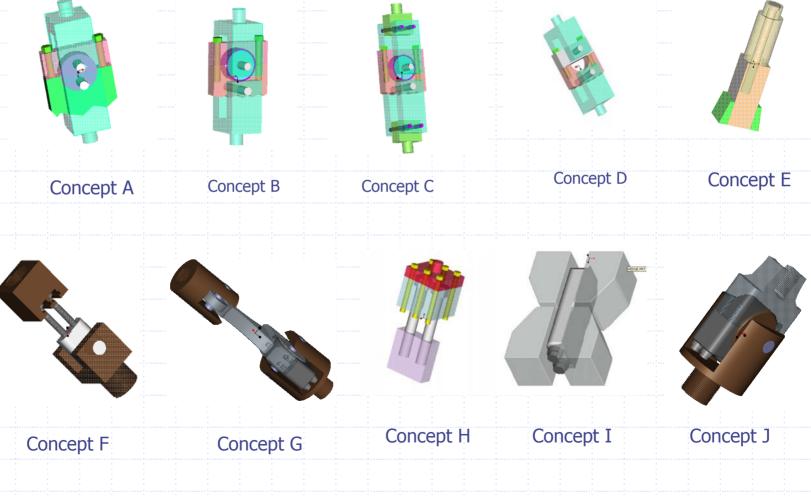
Demands	Requirement	Importance
Demand	Two different set ups, one that will test the main bearing cap and another that will test the connecting rod joints.	10
Demand	Test fixtures should reproduce the failure mode of real components	10
Demand	Design will interface with a fatigue test rig, (e.g. MTS Servohydraulic machine)	10
Demand	Pre-load on the main bearing Cap be 45,000 lbs	10
Demand	Pre-load on the connecting rod be 16,000 lbs	10
Demand	Bolt boss diameter, thread pitch, thread type, counterbore depth, number of engaged threads, bolt preload, and alternating load should be studied	10
Demand	Estimated cost of Hardware (samples will be provided)	8
Final Report_04	0705	

Design Specifications

- Specifications
 - Pre-load requirements
 - 45,000 lb for main bearing cap
 - 16,000 lb for connecting rod
 - Testing for 500,000 cycles
 - Dimensions
 - Seen in engineering drawing(s) of our final selection



Design Generation & Selection







Design Selection

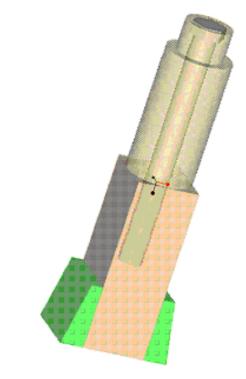
	Cost	Man	Rel	Perf	Cus.S	Total
Α	0.8	0.75	1.05	1.4	2.1	6.1
В	0.8	0.75	4.05	1.4	2.1	6.1
С	1	0.9	1.05	1.4	2.1	6.45
D	0.8	0.7	1.05	1.3	2	5.85
E	1.6	1.35	0.75	1.4	2.1	7.2
F	0.8	0.45	1.2	1.6	2.1	6.15
G	1	0.6	0.6	0.6	0.6	3.4
H	1	1.2	0.75	1.4	2.1	6.45
	1.2	1.05	0.75	1.4	2.1	6.5
J	1.6	1.35	0.75	1.4	2.1	7.2

Each concept is ranked from 1-10. (1 being the worst, and 10 being the best) The ranking is then multiplied by the weighted values below and then added up to show the final total. The concept with the highest total will show what the final design concept should be.



Selection for main bearing cap

Based on design matrix, the final design



- Chosen for ease of manufacturability and simplicity.
- Fixture is small enough to fit within wedges inside of the MTS machine.
 - Top will be screwed into the top portion of the MTS machine

Modifications done to bearing cap selection:



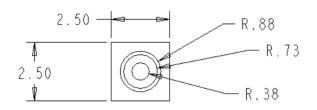
Bolt head of previous design was too large to fit into MTS machine Adapter (yellow) was made to fit fixture (light blue) within MTS machine.

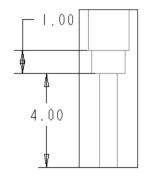
Engine block cut out specimen is in brown, wedges are in gray, and bolt being tested can be seen through the transparent fixture.

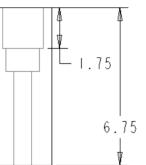


Engineering Drawing / Dimensions of Final Selection

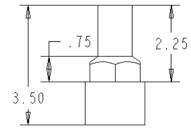
(Main Bearing Cap)



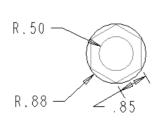


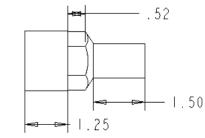


Test Fixture







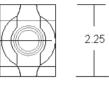


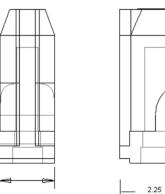


Main Bearing Cap

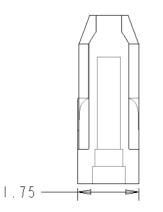
before

1.75 -

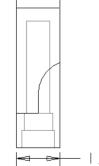










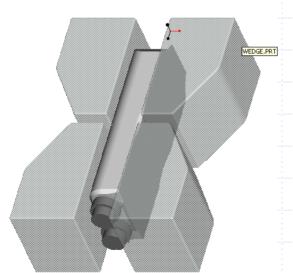






Selection for connecting rod

Based on design matrix, the final design concept is:



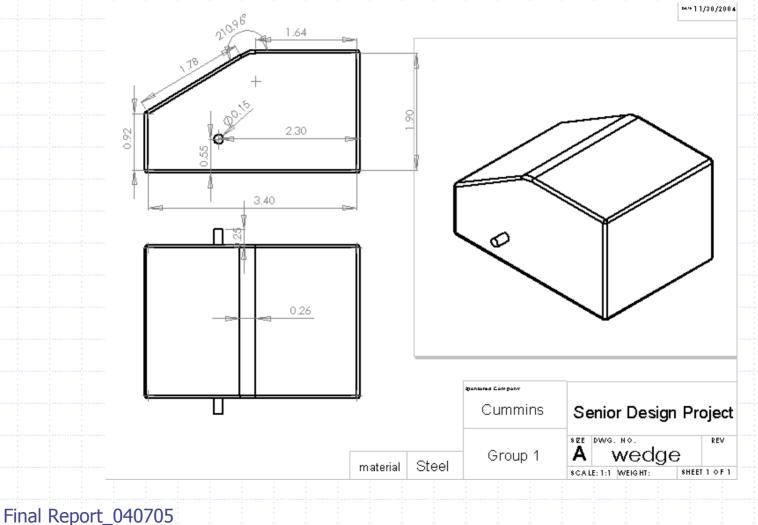
Chosen for ease of manufacturability as well.

Multiple test samples from individual part.

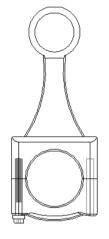
Uses two vice grips for top and bottom connections.



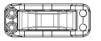
Engineering Drawing / Dimensions of Final Selection (Connecting Rod)



Connecting Rod



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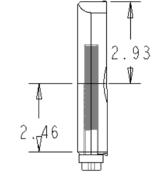




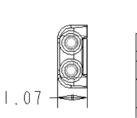
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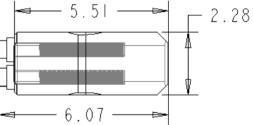


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after









Trip to Bonifay

- Went to Bonifay, Jan 28, 2005
 - Holmes Machine Shop
- Met with Tim Steverson
 - Talked about parts and machining.
 - Minor changes were made
 - Part finishes save money
 - Material 4140 HT steel



cummins

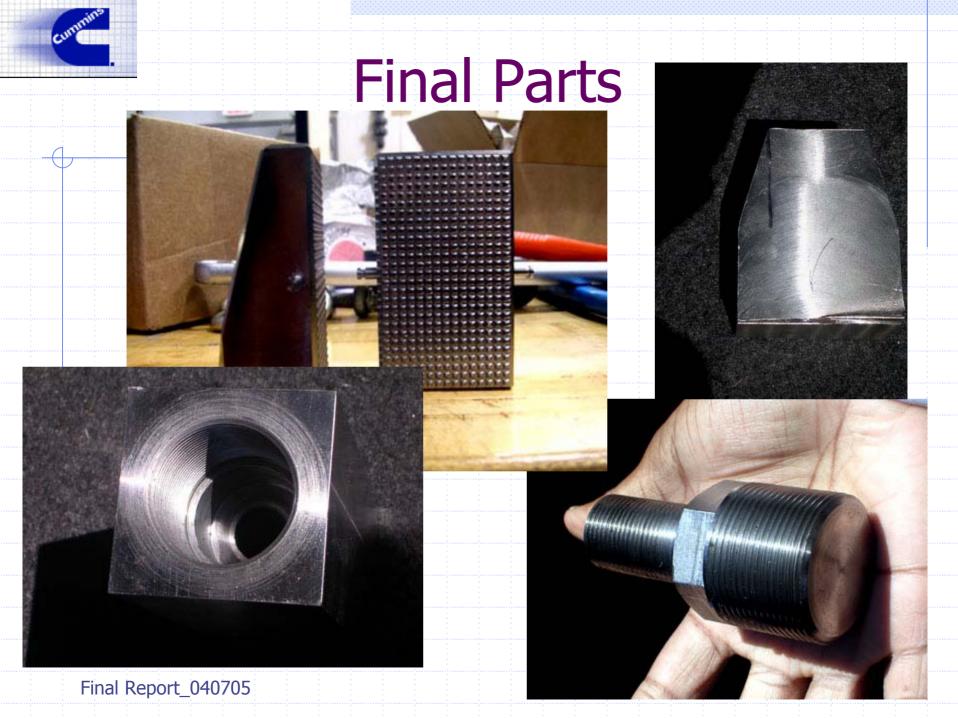
Material and finish changes:

Wedges

- 4140 Steel chosen
 - 311 HB (enough for our testing)
 - Available by Holmes Machine Shop
 - Saved time and money

Finish on Wedges

- Finish was suggested by Bob Walsh (NHMFL)
 - Not feasible with our time & money constraints
- Altered by Holmes Machine Shop
 - Adequate finish for our testing



Costs

<u>i</u> i i			
Qty	Description	Unit price	Total price
4	Wedges w/ pins 4140 HT	\$250.00	\$1,000.00
1	Modify connecting rod	\$200.00	\$200.00
1	Cylinder for fixture	\$125.00	\$125.00
1	Square housing for fixture	\$300.00	\$300.00
		755566	

Total cost \$1625.00

The Engine block samples were machined in the machine shop here at the Engineering School at no cost.



Getting ready for testing

applying torque to bolts:



where T is the torque, k is the torque coefficient, d is the bolt diameter, and F is the preload value

	Connecting Rod	Main Bearing Cap
Pre-Load, F (lbs)	16,000	45,000
Bolt diameter, D (mm)		20
Torque coefficient, k	0.21	0.21
Calculated Torque (ft-lbs)	130	620 → 330
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Final

Torque





The connecting rods were torqued at the NHMFL, while we had to go to Florida Rock to torque the main bearing cap bolts. Final Report_040705





- Four test
- Results
 - Connecting Rod
 - Main Bearing Cap
- Recommendations
 - Test setup
- Conclusion





Connecting Rod Test #1 (REBD)[§]

- Torque applied per bolt 65 lb-ft
- Tension & Compression @ 3 Hz
- Applied load 8,000 lbs
- Amplitude of 16,000 lbs
- Specimen slipped 3 times
- 1.3 million cycles total
- Specimen did not break



Fension

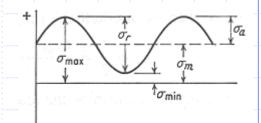
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Stress

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Connecting Rod Test #2 (JB)

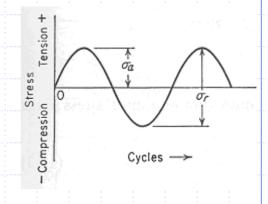
- Torque applied per bolt 130 lb-ft
- Tested only in tension @ 3 Hz
- Initial load 16,000 lbs
- Final load 24,000 lbs
- Specimen slipped twice
- 1 million cycles total
- Wedge failed.





Main Bearing Cap Test #3

- Engine block was modified
- Torque applied 300 lb-ft
- Tension & Compression @ 2 Hz
- Amplitude of 45,000 lbs
- 1 thousand cycles total
- Specimen failed unexpectedly

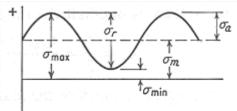






Main Bearing Cap Test #4

- Engine block modified
- Torque applied 330 lb-ft
- Tension only, @ 2 Hz
- Amplitude of 22,500 lbs
- 10 thousand cycles total
- Specimen failed



^îσ_{min} Cycles →





Results

Connecting Rod

- JB tested up to 1.3 million cycles
 - Specimen did not fail
- REBD tested up to 980,389 cycles
 - Wedge failed

Main Bearing Cap

- First set up failed at 1,000 cycles
 Second set up failed at 10,000 cycles
- Second set up failed at 10,000 cycles





Recommendations

Make wedges out of harder materials

- High Carbon Steels
- Tool Steel

Decrease the wedges thickness

Allows for a larger sample





Conclusions

Our objectives were;

- Design a fixture
- Test & Evaluate threaded joints

Design process

- Manufactured test fixture
- Performed 4 test
 - 2 test on the connecting rod
 - 2 test on the main bearing cap
- Threads didn't fail





Acknowledgements

Cummins

- Bob Tickel
- Dave Parsons
- Dr. Luongo
- Dr. Kalu
- ♦ NHMFL
 - Bob Walsh
 - Chika Okoro
- Holmes Machine Shop
- Keith Larson
- Florida Rock



References

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- Norton, Robert L. <u>Machine Design: An Integrated Approach</u>. Upper Saddle River, NJ: Prentice Hall, 2000.
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